CE – 842, Credits: 3 + 0, Semester: Spring 2022

Performance-based Seismic Design of Structures

Department of Structural Engineering

National University of Sciences and Technology (NUST)



Seismic Analysis & Design of Buildings using IBC-2021 (BCP-2021) & ASCE 7-16



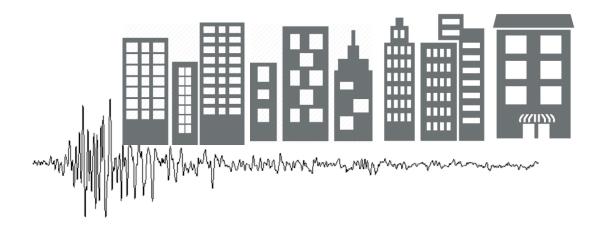
Fawad A. Najam, PE, PhD.

Assistant Professor (Structural Engineering)
Department of Structural Engineering
NUST Institute of Civil Engineering (NICE)
National University of Sciences and Technology (NUST)
H-12 Islamabad, Pakistan
Cell: 92-334-5192533, Email: fawad@nice.nust.edu.pk

Contents

- Seismic Analysis & Design of Buildings using IBC-2021 (BCP-2021) & ASCE 7-16
 - Equivalent Lateral Force (ELF) Procedure
 - Modal Response Spectrum Analysis Procedure
 - Modal Response History Analysis Procedure

Seismic Hazard Assessment



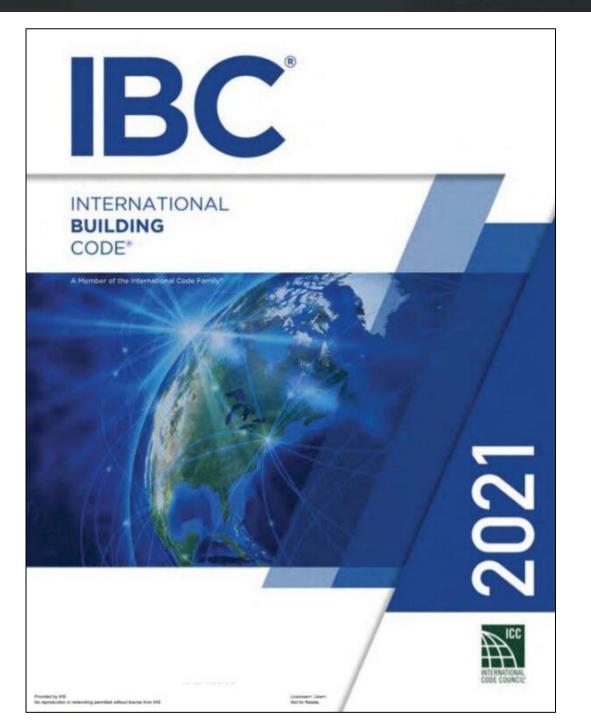
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Dr. Fawad A. Najam

Department of Structural Engineering
NUST Institute of Civil Engineering (NICE)
National University of Sciences and Technology (NUST)
H-12 Islamabad, Pakistan

Cell: 92-334-5192533, Email: fawad@nice.nust.edu.pk

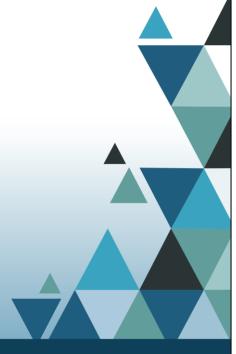












BUILDING CODE OF PAKISTAN-2021 **ASCE 7-16**

ASCE STANDARD

ASCE/SEI

7-16

Minimum Design Loads and Associated Criteria for Buildings and Other Structures





IBC-2018

[A] 104.11 Alternative materials, design and methods of construction and equipment. The provisions of this code are not intended to prevent the installation of any material or to prohibit any design or method of construction not specifically prescribed by this code, provided that any such alternative has been approved. An alternative material, design or method of construction shall be approved where the building official finds that the proposed design is satisfactory and complies with the intent of the provisions of this code, and that the material, method or work offered is, for the purpose intended, not less than the equivalent of that prescribed in this code in quality, strength, effectiveness, fire resistance, durability and safety. Where the alternative material, design or method of construction is not approved, the building official shall respond in writing, stating the reasons why the alternative was not approved.

IBC-2021

[A] 104.11 Alternative materials, design and methods of construction and equipment. The provisions of this code are not intended to prevent the installation of any material or to prohibit any design or method of construction not specifically prescribed by this code, provided that any such alternative has been *approved*. An alternative material, design or method of construction shall be *approved* where the *building official* finds that the proposed alternative meets all of the following:

- 1. The alternative material, design or method of construction is satisfactory and complies with the intent of the provisions of this code,
- 2. The material, method or work offered is, for the purpose intended, not less than the equivalent of that prescribed in this code as it pertains to the following:
 - 2.1. Quality.
 - 2.2. Strength.
 - 2.3. Effectiveness.
 - 2.4. Fire resistance.
 - 2.5. Durability.
 - 2.6. Safety.

Where the alternative material, design or method of construction is not approved, the *building official* shall respond in writing, stating the reasons why the alternative was not approved.

BCP-2021

104.11 Alternative materials, design and methods of construction and equipment. The provisions of this code are not intended to prevent the installation of any material or to prohibit any design or method of construction not specifically prescribed by this code, provided that any such alternative has been *approved*. An alternative material, design or method of construction shall be *approved* where *AHJ* takes help from experts (*Registered design professionals*) to review and confirm that the proposed alternative meets all of the following:

- 1. The alternative material, design or method of construction is satisfactory and complies with the intent of the provisions of this code,
- 2. The material, method or work offered is, for the purpose intended, not less than the equivalent of that prescribed in this code as it pertains to the following:
 - 2.1. Quality.
 - 2.2. Strength.
 - 2.3. Effectiveness.
 - 2.4. Fire resistance.
 - 2.5. Durability.
 - 2.6. Safety.

Where the alternative material, design or method of construction is not approved, *AHJ* shall respond in writing, stating the reasons why the alternative was not approved.

Seismic Analysis & Design of Buildings using IBC-2021 (BCP-2021) & ASCE 7-16

Basic Input Information:

- · Configuration/geometry of building
- · Initial cross-sectional and material properties
- · Intended use of building
- · Site Class
- · Gravity load resisting system
- · Lateral load resisting System

Basic Steps: Common to all Seismic Analysis Procedures

Step 1: Establish the "Risk Category" of the building. Based on the occupancy/Intended use of building Sdect the category from Table 1.5-1 (ASCE 7-16)

Table 1.5-1 Risk Category of Buildings and Other Structures for Flood, Wind, Snow, Earthquake, and Ice Loads

| Use or Occupancy of Buildings and Structures | Risk Category |
|---|---------------|
| Buildings and other structures that represent low risk to human life in the event of failure | Ι |
| All buildings and other structures except those listed in Risk Categories I, III, and IV | II |
| Buildings and other structures, the failure of which could pose a substantial risk to human life | III |
| Buildings and other structures, not included in Risk Category IV, with potential to cause a substantial economic impact and/or mass disruption of day-to-day civilian life in the event of failure | |
| Buildings and other structures not included in Risk Category IV (including, but not limited to, facilities that manufacture, process, handle, store, use, or dispose of such substances as hazardous fuels, hazardous chemicals, hazardous waste, or explosives) containing toxic or explosive substances where the quantity of the material exceeds a threshold quantity | |

established by the Authority Having Jurisdiction and is

sufficient to pose a threat to the public if released^a

Selection of Risk Category

IV

Buildings and other structures designated as essential facilities Buildings and other structures, the failure of which could pose a substantial hazard to the community Buildings and other structures (including, but not limited to, facilities that manufacture, process, handle, store, use, or dispose of such substances as hazardous fuels, hazardous chemicals, or hazardous waste) containing sufficient quantities of highly toxic substances where the quantity of the material exceeds a threshold quantity established by the Authority Having Jurisdiction and is sufficient to pose a threat to the public if released^a

Buildings and other structures required to maintain the

functionality of other Risk Category IV structures

^aBuildings and other structures containing toxic, highly toxic, or explosive substances shall be eligible for classification to a lower Risk Category if it can be demonstrated to the satisfaction of the Authority Having Jurisdiction by a hazard assessment as described in Section 1.5.3 that a release of the substances is commensurate with the risk associated with that Risk Category.

Step 2: Determine the "Ground Motion Parameters, So and Si" of the Site.

a) Use the hazard maps to determine "Risk-targetted maximum considered earthquake (MCER) spectral response acceleration parameters for short periods (Ss) and at 1 sec (S1).

For US, S_s — Figures 22-1 to 22-8 (ASCE 7-16) S₁ — Figures 22-2 to 22-8

b) Select Site Coefficients Fa and Fv

 $F_a \rightarrow Table \ 11.4-1 \ [vsing site class and S_s] \ F_V \rightarrow Table \ 11.4-2 \ [vsing site class and S_1] \ Determine adjusted ground Motion parameters.$

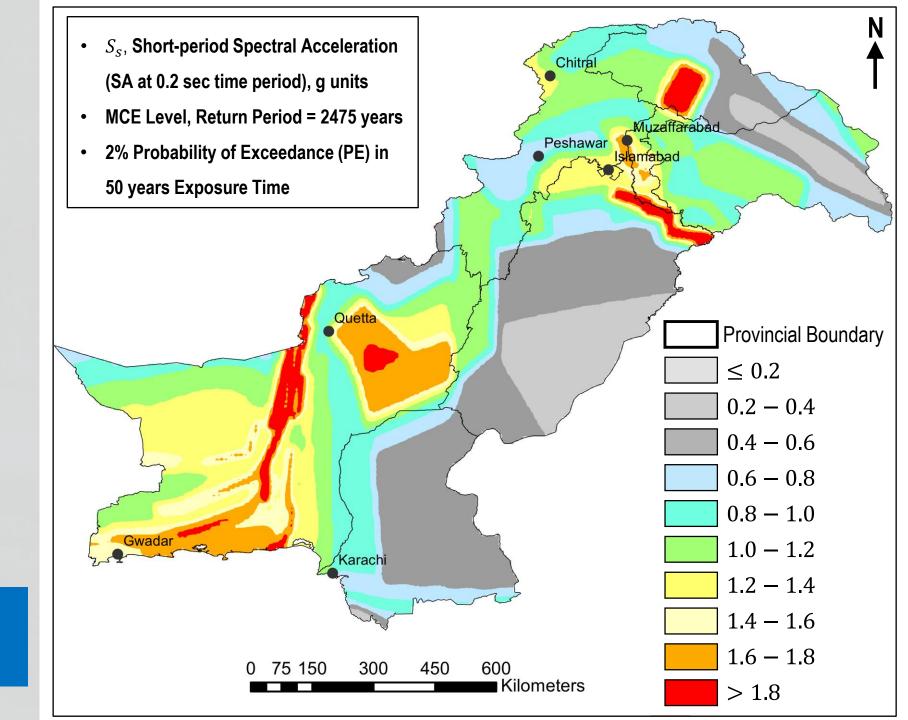
$$S_{MS} = F_a S_S$$
 (11.4-1) (ASCE 7-16)
 $S_{M1} = F_v S_1$ (11.4-2)

Ground Motion

Parameters for Pakistan

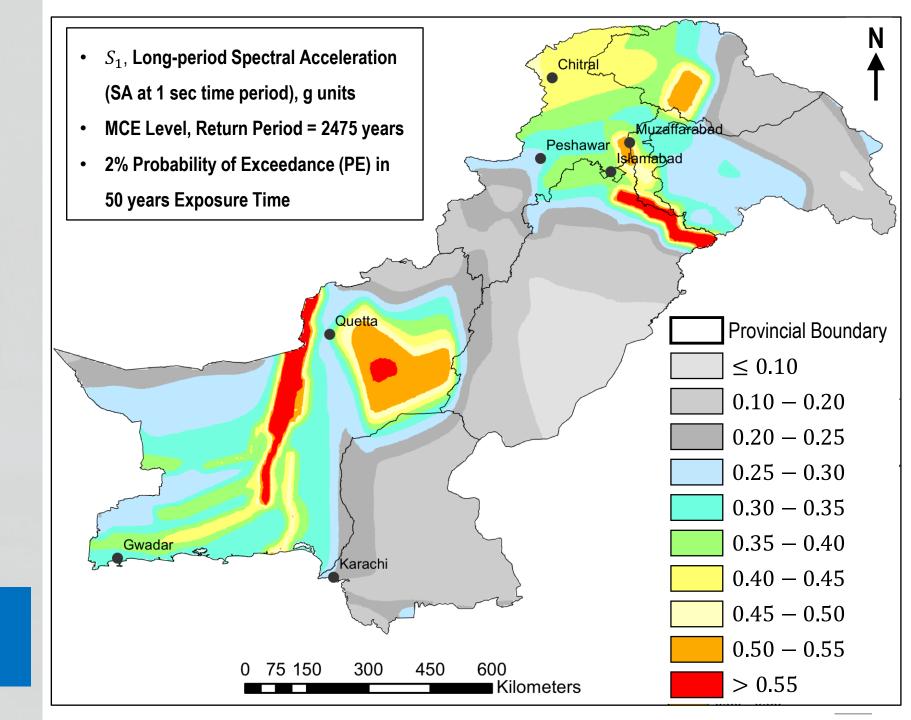
(BCP-2021)

For tabular values: www.fawadnajam.com/bcp-2021



Ground Motion
Parameters for Pakistan
(BCP-2021)

For tabular values: www.fawadnajam.com/bcp-2021



Site Coefficients

Table 11.4-1 Short-Period Site Coefficient, F_a

Mapped Risk-Targeted Maximum Considered Earthquake (MCE_R) Spectral Response Acceleration Parameter at Short Period

| Site Class | ${\cal S}_{\cal S} \le 0.25$ | <i>S</i> _S = 0.5 | S _S = 0.75 | <i>S_S</i> = 1.0 | <i>S</i> _S = 1.25 | <i>S</i> _S ≥ 1.5 |
|---------------|------------------------------|-----------------------------|-----------------------|----------------------------|------------------------------|-----------------------------|
| A | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 |
| В | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 |
| C | 1.3 | 1.3 | 1.2 | 1.2 | 1.2 | 1.2 |
| D | 1.6 | 1.4 | 1.2 | 1.1 | 1.0 | 1.0 |
| E | 2.4 | 1.7 | 1.3 | See | See | See |
| | | | | Section | Section | Section |
| | | | | 11.4.8 | 11.4.8 | 11.4.8 |
| F | See | See | See | See | See | See |
| | Section | Section | Section | Section | Section | Section |
| | 11.4.8 | 11.4.8 | 11.4.8 | 11.4.8 | 11.4.8 | 11.4.8 |

Note: Use straight-line interpolation for intermediate values of S_s .

Table 11.4-2 Long-Period Site Coefficient, F_{ν}

Mapped Risk-Targeted Maximum Considered Earthquake (MCE_R) Spectral Response Acceleration Parameter at 1-s Period

| Site Class | $S_1 \leq 0.1$ | $S_1 = 0.2$ | $S_1 = 0.3$ | $S_1 = 0.4$ | $S_1 = 0.5$ | $S_1 \ge 0.6$ |
|---------------|----------------|-------------|-------------|-------------|-------------|---------------|
| A | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 |
| В | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 |
| C | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.4 |
| D | 2.4 | 2.2^{a} | 2.0^{a} | 1.9^{a} | 1.8^{a} | 1.7^{a} |
| E | 4.2 | See | See | See | See | See |
| | | Section | Section | Section | Section | Section |
| | | 11.4.8 | 11.4.8 | 11.4.8 | 11.4.8 | 11.4.8 |
| F | See | See | See | See | See | See |
| | Section | Section | Section | Section | Section | Section |
| | 11.4.8 | 11.4.8 | 11.4.8 | 11.4.8 | 11.4.8 | 11.4.8 |

Note: Use straight-line interpolation for intermediate values of S_1 .

11.4.8 Site-Specific Ground Motion Procedures.

^aAlso, see requirements for site-specific ground motions in Section 11.4.8.

C) Determine design spectral accelerations.

$$S_{DS} = \frac{2}{3} S_{MS} (11.4-3)$$

 $S_{D1} = \frac{2}{3} S_{M1} (11.4-4)$ [ASCE 7-16]

Step 3: Determine Importance Factor(Ie)

Based on Risk Category, select seismic importance

factor (Ie) from Table 1.5-2 [ASCE 7-16]

Step 4: Determine the Seismic Design Category (SDC) of your Structure.

Based on Risk Category and values of SDS and SD19 establish the SDC using Tables 11.6-1 and 11.6-2 and Section 11.6 [ASCE 7-16]

Importance Factor

Table 1.5-2 Importance Factors by Risk Category of Buildings and Other Structures for Snow, Ice, and Earthquake Loads

| Risk Category from Table 1.5-1 | Snow Importance Factor, <i>I_s</i> | Ice Importance Factor— Thickness, <i>I</i> ; | Ice Importance Factor—Wind, I_w | Seismic Importance Factor, <i>I_e</i> |
|--------------------------------------|--|--|-----------------------------------|---|
| I | 0.80 | 0.80 | 1.00 | 1.00 |
| II | 1.00 | 1.00 | 1.00 | 1.00 |
| III | 1.10 | 1.15 | 1.00 | 1.25 |
| IV | 1.20 | 1.25 | 1.00 | 1.50 |

Note: The component importance factor, I_p , applicable to earthquake loads, is not included in this table because it depends on the importance of the individual component rather than that of the building as a whole, or its occupancy. Refer to Section 13.1.3.

11.6 SEISMIC DESIGN CATEGORY

Structures shall be assigned a Seismic Design Category in accordance with this section.

Risk Category I, II, or III structures located where the mapped spectral response acceleration parameter at 1-s period, S_1 , is greater than or equal to 0.75 shall be assigned to Seismic Design Category E. Risk Category IV structures located where the mapped spectral response acceleration parameter at 1-s period, S_1 , is greater than or equal to 0.75 shall be assigned to Seismic Design Category F. All other structures shall be assigned to a Seismic Design Category based on their Risk Category and the design spectral response acceleration parameters, S_{DS} and S_{D1} , determined in accordance with Section 11.4.5. Each building and structure shall be assigned to the more severe Seismic Design Category in accordance with Table 11.6-1 or 11.6-2, irrespective

of the fundamental period of vibration of the structure, T. The provisions in Chapter 19 shall not be used to modify the spectral response acceleration parameters for determining Seismic Design Category.

Where S_1 is less than 0.75, the Seismic Design Category is permitted to be determined from Table 11.6-1 alone where all of the following apply:

- 1. In each of the two orthogonal directions, the approximate fundamental period of the structure, T_a , determined in accordance with Section 12.8.2.1 is less than $0.8T_s$, where T_s is determined in accordance with Section 11.4.6.
- 2. In each of two orthogonal directions, the fundamental period of the structure used to calculate the story drift is less than T_s .

- 3. Eq. (12.8-2) is used to determine the seismic response coefficient C_s .
- 4. The diaphragms are rigid in accordance with Section 12.3; or, for diaphragms that are not rigid, the horizontal distance between vertical elements of the seismic force-resisting system does not exceed 40 ft (12.192 m).

Where the alternate simplified design procedure of Section 12.14 is used, the Seismic Design Category is permitted to be determined from Table 11.6-1 alone, using the value of S_{DS} determined in Section 12.14.8.1, except that where S_1 is greater than or equal to 0.75, the Seismic Design Category shall be E.

Seismic Design Category

TABLE 11.6-1 Seismic Design Category Based on Short-Period Response Acceleration Parameter

| _ | Risk Cat | egory |
|---------------------------|----------------|-------|
| Value of S_{DS} | l or II or III | IV |
| $S_{DS} < 0.167$ | A | A |
| $0.167 \le S_{DS} < 0.33$ | В | C |
| $0.33 \le S_{DS} < 0.50$ | C | D |
| $0.50 \le S_{DS}$ | D | D |

TABLE 11.6-2 Seismic Design Category Based on 1-s Period Response Acceleration Parameter

| | Risk Cat | egory |
|----------------------------|----------------|-------|
| Value of S_{D1} | l or II or III | IV |
| $S_{D1} < 0.067$ | A | A |
| $0.067 \le S_{D1} < 0.133$ | В | C |
| $0.133 \le S_{D1} < 0.20$ | C | D |
| $0.20 \le S_{D1}$ | D | D |

Step 5: Select the Structural System.

a) Check Structural system limitations and Structural height

limits using Table 12:2-1 [ASCE 7-16]

For example, For concrete SMRFs (C.5) -> NL (for all SDCs)

Not limited

For Concrete IMRF (C.6) -> NL (for SDC B,c)

NP (for SDC D,E,F)

Not permitted

For Steel special truss moment

Not permitted

NP -> For SDCF

b) Select the values of

(i) Response modification factor, R

(ii) Over strength factor, Do

(iii) Deflection Amplification Factor, Cd

Table 12.2-1 Design Coefficients and Factors for Seismic Force-Resisting Systems

Structural System Limitations Including Structural Height, h_n (ft) Limits^d

Selection of Seismic Design Parameters

| | ASCE 7 Section Where Detailing | Response | O | Deflection | | Seismic | Design C | ategory | | |
|--|-----------------------------------|-------------------------------|------|------------|-------|----------------|----------|----------|----------|--|
| Name | Factor, Ω_0^b | Amplification Factor, C_d^c | В | С | D^e | E ^e | F' | | | |
| | | | | | | | | | | |
| | 14.2 | 5 | 21/2 | 5 | NL | NL | 160 | 160 | 100 | |
| | 14.2 | 4 | 21/2 | 4 | NL | NL | NP | NP | NP | |
| 3. Detailed plain concrete shear walls ^g | 14.2 | 2 | 21/2 | 2 | NL | NP | NP | NP | NP | |
| 4. Ordinary plain concrete shear walls ^g | 14.2 | 11/2 | 21/2 | 11/2 | NL | NP | NP | NP | NP | |
| 5. Intermediate precast shear walls ^g | 14.2 | 4 | 21/2 | 4 | NL | NL | 40^{i} | 40^{i} | 40^i | |
| 6. Ordinary precast shear walls ^g | 14.2 | 3 | 21/2 | 3 | NL | NP | NP | NP | NP | |
| 7. Special reinforced masonry shear walls | 14.4 | 5 | 21/2 | 31/2 | NL | NL | 160 | 160 | 100 | |
| 8. Intermediate reinforced masonry shear walls | 14.4 | 31/2 | 21/2 | 21/4 | NL | NL | NP | NP | NP | |
| 9. Ordinary reinforced masonry shear walls | 14.4 | 2 | 21/2 | 13/4 | NL | 160 | NP | NP | NP | |
| 10. Detailed plain masonry shear walls | 14.4 | 2 | 21/2 | 13/4 | NL | NP | NP | NP | NP | |
| 11. Ordinary plain masonry shear walls | 14.4 | 11/2 | 21/2 | 11/4 | NL | NP | NP | NP | NP | |
| | 14.4 | 11/2 | 21/2 | 13/4 | NL | NP | NP | NP | NP | |
| 13. Ordinary reinforced AAC masonry shear walls | 14.4 | 2 | 21/2 | 2 | NL | 35 | NP | NP | NP | |
| | 14.4 | 11/2 | 21/2 | 11/2 | NL | NP | NP | NP | NP | |
| | 14.5 | 61/2 | 3 | 4 | NL | NL | 65 | 65 | 65 | |
| 16. Light-frame (cold-formed steel) walls sheathed with wood structural panels | 14.1 | 61/2 | 3 | 4 | NL | NL | 65 | 65 | 65 | |
| | 14.1 and 14.5 | 2. | 21/2 | 2 | NL | NL | 35 | NP | NP | |
| | | | | 31/2 | NL | NL | 65 | 65 | 65 | |
| B. BUILDING FRAME SYSTEMS | | | | | | | | | | |
| 1. Steel eccentrically braced frames | 14.1 | 8 | 2 | 4 | NL | NL | 160 | 160 | 100 | |
| 2. Steel special concentrically braced frames | 14.1 | 6 | 2 | 5 | NL | NL | 160 | 160 | 100 | |
| 3. Steel ordinary concentrically braced frames | 14.1 | 31/4 | 2 | 31/4 | NL | NL | 35^{j} | 35^{j} | NP^{j} | |
| 4. Special reinforced concrete shear walls ^{g,h} | 14.2 | 6 | 21/2 | 5 | NL | NL | 160 | 160 | 100 | |
| 5. Ordinary reinforced concrete shear walls ^g | 14.2 | 5 | 21/2 | 41/2 | NL | NL | NP | NP | NP | |
| 6. Detailed plain concrete shear walls ^g | | 2 | 21/2 | 2 | NL | NP | NP | NP | NP | |
| 7. Ordinary plain concrete shear walls ^g | 14.2 | 11/2 | 21/2 | 11/2 | NL | NP | NP | NP | NP | |
| | 14.2 | 5 | 21/2 | 41/2 | NL | NL | 40^i | 40^{i} | 40^i | |
| | 14.2 | 4 | 21/2 | 4 | NL | NP | NP | NP | NP | |
| | 14.3 | 8 | 21/2 | 4 | NL | NL | 160 | 160 | 100 | |
| | | 5 | 2 | 41/2 | NL | NL | 160 | 160 | 100 | |
| | | 3 | | 3 | NL | NL | NP | NP | NP | |
| | 14.3 | 61/2 | 21/2 | 51/2 | NL | NL | 160 | 160 | 100 | |
| | | | | 5 | NL | NL | 160 | 160 | 100 | |
| | | _ | | 41/2 | NL | NL | NP | NP | NP | |
| | | | | 4 | NL | NL | 160 | 160 | 100 | |
| 17. Intermediate reinforced masonry shear walls | 14.4 | 4 | 21/2 | 4 | NL | NL | NP | NP | NP | |

Selection of Seismic Design Parameters

| 18. Ordinary reinforced masonry shear walls | 14.4 | 2 | 21/2 | 2 | NL | 160 | NP | NP | NP |
|---|-------------------|----------------|---------------------------|------|-----|-----|----------|----------|--------|
| 19. Detailed plain masonry shear walls | 14.4 | 2 | 21/2 | 2 | NL | NP | NP | NP | NP |
| 20. Ordinary plain masonry shear walls | 14.4 | 11/2 | 21/2 | 11/4 | NL | NP | NP | NP | NP |
| 21. Prestressed masonry shear walls | 14.4 | 11/2 | 21/2 | 13/4 | NL | NP | NP | NP | NP |
| 22. Light-frame (wood) walls sheathed with wood structural panels rated for shear resistance | 14.5 | 7 | 21/2 | 41/2 | NL | NL | 65 | 65 | 65 |
| 23. Light-frame (cold-formed steel) walls sheathed with wood structural panels rated for shear resistance or steel sheets | 14.1 | 7 | 21/2 | 41/2 | NL | NL | 65 | 65 | 65 |
| 24. Light-frame walls with shear panels of all other materials | 14.1 and 14.5 | 21/2 | 21/2 | 21/2 | NL | NL | 35 | NP | NP |
| 25. Steel buckling-restrained braced frames | 14.1 | 8 | $\frac{2^{1/2}}{2^{1/2}}$ | 5 | NL | NL | 160 | 160 | 100 |
| 26. Steel special plate shear walls | 14.1 | 7 | 2 | 6 | NL | NL | 160 | 160 | 100 |
| C. MOMENT-RESISTING FRAME SYSTEMS | | | | | | | | | |
| 1. Steel special moment frames | 14.1 and 12.2.5.5 | 8 | 3 | 51/2 | NL | NL | NL | NL | NL |
| 2. Steel special truss moment frames | 14.1 | 7 | 3 | 51/2 | NL | NL | 160 | 100 | NP |
| 3. Steel intermediate moment frames | 12.2.5.7 and 14.1 | 41/2 | 3 | 4 | NL | NL | 35^{k} | NP^k | NP^k |
| 4. Steel ordinary moment frames | 12.2.5.6 and 14.1 | 31/2 | 3 | 3 | NL | NL | NP^l | NP^{l} | NP^l |
| 5. Special reinforced concrete moment frames ^m | 12.2.5.5 and 14.2 | 8 | 3 | 51/2 | NL | NL | NL | NL | NL |
| 6. Intermediate reinforced concrete moment frames | 14.2 | 5 | 3 | 41/2 | NL | NL | NP | NP | NP |
| 7. Ordinary reinforced concrete moment frames | 14.2 | 3 | 3 | 2½ | NL | NP | NP | NP | NP |
| 8. Steel and concrete composite special moment frames | 12.2.5.5 and 14.3 | 8 | 3 | 51/2 | NL | NL | NL | NL | NL |
| 9. Steel and concrete composite intermediate moment frames | 14.3 | 5 | 3 | 41/2 | NL | NL | NP | NP | NP |
| 10. Steel and concrete composite partially restrained moment frames | 14.3 | 6 | 3 | 51/2 | 160 | 160 | 100 | NP | NP |
| 11. Steel and concrete composite ordinary moment frames | 14.3 | 3 | 3 | 21/2 | NL | NP | NP | NP | NP |
| 12. Cold-formed steel—special bolted moment frame ⁿ | 14.1 | 31/2 | 30 | 3½ | 35 | 35 | 35 | 35 | 35 |
| D. DUAL SYSTEMS WITH SPECIAL MOMENT FRAMES CAPABLE | 12.2.5.1 | | | | | | | | |
| OF RESISTING AT LEAST 25% OF PRESCRIBED SEISMIC FORCES | | | | | | | | | |
| 1. Steel eccentrically braced frames | 14.1 | 8 | 21/2 | 4 | NL | NL | NL | NL | NL |
| 2. Steel special concentrically braced frames | 14.1 | 7 | 21/2 | 51/2 | NL | NL | NL | NL | NL |
| 3. Special reinforced concrete shear walls ^{g,h} | 14.2 | 7 | 21/2 | 51/2 | NL | NL | NL | NL | NL |
| 4. Ordinary reinforced concrete shear walls ^g | 14.2 | 6 | 21/2 | 5 | NL | NL | NP | NP | NP |
| 5. Steel and concrete composite eccentrically braced frames | 14.3 | 8 | 21/2 | 4 | NL | NL | NL | NL | NL |
| 6. Steel and concrete composite special concentrically braced frames | 14.3 | 6 | 21/2 | 5 | NL | NL | NL | NL | NL |
| 7. Steel and concrete composite plate shear walls | 14.3 | $7\frac{1}{2}$ | 21/2 | 6 | NL | NL | NL | NL | NL |
| 8. Steel and concrete composite special shear walls | 14.3 | 7 | 21/2 | 6 | NL | NL | NL | NL | NL |
| 9. Steel and concrete composite ordinary shear walls | 14.3 | 6 | 21/2 | 5 | NL | NL | NP | NP | NP |
| 10. Special reinforced masonry shear walls | 14.4 | 51/2 | 3 | 5 | NL | NL | NL | NL | NL |
| 11. Intermediate reinforced masonry shear walls | 14.4 | 4 | 3 | 31/2 | NL | NL | NP | NP | NP |
| 12. Steel buckling-restrained braced frames | 14.1 | 8 | 21/2 | 5 | NL | NL | NL | NL | NL |
| 13. Steel special plate shear walls | 14.1 | 8 | 21/2 | 61/2 | NL | NL | NL | NL | NL |
| E. DUAL SYSTEMS WITH INTERMEDIATE MOMENT FRAMES | 12.2.5.1 | | | | | | | | |
| CAPABLE OF RESISTING AT LEAST 25% OF PRESCRIBED | | | | | | | | | |
| SEISMIC FORCES | | | | | | | | | |
| 1. Steel special concentrically braced frames ^p | 14.1 | 6 | 21/2 | 5 | NL | NL | 35 | NP | NP |
| 2. Special reinforced concrete shear walls ^{g,h} | 14.2 | 61/2 | 21/2 | 5 | NL | NL | 160 | 100 | 100 |
| 3. Ordinary reinforced masonry shear walls | 14.4 | 3 | 3 | 21/2 | NL | 160 | NP | NP | NP |
| 4. Intermediate reinforced masonry shear walls | 14.4 | 31/2 | 3 | 3 | NL | NL | NP | NP | NP |

continues

Table 12.2-1 (Continued) Design Coefficients and Factors for Seismic Force-Resisting Systems

| | | | | | Structural System Limitations Including Structural Height, h_n (ft) Limits ^d | | | | | |
|--|--------------------------------|--|---------------------------------------|-------------------------------|---|----|-----------------|----------|-----------------|--|
| | ASCE 7 Section Where Detailing | Response | | Deflection | Seismic Design Category | | | | | |
| Seismic Force-Resisting System | Requirements Are Specified | Modification Coefficient, <i>R</i> ^a | Overstrength Factor, $\Omega_0^{\ b}$ | Amplification Factor, C_d^c | В | С | De | E | F ^f | |
| 5. Steel and concrete composite special concentrically braced frames | 14.3 | 5½ | 21/2 | 4½ | NL | NL | 160 | 100 | NP | |
| 6. Steel and concrete composite ordinary braced frames | 14.3 | 31/2 | 21/2 | 3 | NL | NL | NP | NP | NP | |
| 7. Steel and concrete composite ordinary shear walls | 14.3 | 5 | 3 | 41/2 | NL | NL | NP | NP | NP | |
| 8. Ordinary reinforced concrete shear walls ^g | 14.2 | 5½ | 21/2 | 41/2 | NL | NL | NP | NP | NP | |
| F. SHEAR WALL-FRAME INTERACTIVE SYSTEM WITH ORDINARY REINFORCED CONCRETE MOMENT FRAMES AND ORDINARY REINFORCED CONCRETE SHEAR WALLS ⁸ | 12.2.5.8 and 14.2 | 4½ | 21/2 | 4 | NL | NP | NP | NP | NP | |
| G. CANTILEVERED COLUMN SYSTEMS DETAILED TO CONFORM TO THE REQUIREMENTS FOR: | 12.2.5.2 | | | | | | | | | |
| 1. Steel special cantilever column systems | 14.1 | 21/2 | 11/4 | 21/2 | 35 | 35 | 35 | 35 | 35 | |
| 2. Steel ordinary cantilever column systems | 14.1 | 11/4 | 11/4 | 11/4 | 35 | 35 | NP^l | NP^{l} | NP^l | |
| 3. Special reinforced concrete moment frames ^m | 12.2.5.5 and 14.2 | 21/2 | 11/4 | 21/2 | 35 | 35 | 35 | 35 | 35 | |
| 4. Intermediate reinforced concrete moment frames | 14.2 | 11/2 | 11/4 | 11/2 | 35 | 35 | NP | NP | NP | |
| 5. Ordinary reinforced concrete moment frames | 14.2 | 1 | 11/4 | 1 | 35 | NP | NP | NP | NP | |
| 6. Timber frames | 14.5 | 11/2 | 11/2 | 11/2 | 35 | 35 | 35 | NP | NP | |
| H. STEEL SYSTEMS NOT SPECIFICALLY DETAILED FOR SEISMIC RESISTANCE, EXCLUDING CANTILEVER COLUMN SYSTEMS | 14.1 | 3 | 3 | 3 | NL | NL | NP | NP | NP | |

^aResponse modification coefficient, R, for use throughout the standard. Note that R reduces forces to a strength level, not an allowable stress level.

^bWhere the tabulated value of the value of Ω_0 , is greater than or equal to $2\frac{1}{2}$, Ω_0 is permitted to be reduced by subtracting the value of 1/2 for structures with flexible diaphragms. ^cDeflection amplification factor, C_d , for use in Sections 12.8.6, 12.8.7, and 12.9.1.2. C_d NL = Not Limited, and NP = Not Permitted. For metric units, use 30.5 m for 100 ft and use 48.8 m for 160 ft.

^eSee Section 12.2.5.4 for a description of seismic force-resisting systems limited to buildings with a structural height, h_n , of 240 ft (73.2 m) or less.

See Section 12.2.5.4 for seismic force-resisting systems limited to buildings with a structural height, h_n , of 160 ft (48.8 m) or less.

^gIn Section 2.3 of ACI 318. A shear wall is defined as a structural wall.

^hIn Section 2.3 of ACI 318. The definition of "special structural wall" includes precast and cast-in-place construction.

An increase in structural height, h_n , to 45 ft (13.7 m) is permitted for single-story storage warehouse facilities. Steel ordinary concentrically braced frames are permitted in single-story buildings up to a structural height, h_n , of 60 ft (18.3 m) where the dead load of the roof does not exceed 20 lb/ft² (0.96 kN/m²) and in penthouse structures.

^kSee Section 12.2.5.7 for limitations in structures assigned to Seismic Design Categories D, E, or F.

See Section 12.2.5.6 for limitations in structures assigned to Seismic Design Categories D, E, or F.

^mIn Section 2.3 of ACI 318. The definition of "special moment frame" includes precast and cast-in-place construction.

[&]quot;Cold-formed steel—special bolted moment frames shall be limited to one story in height in accordance with ANSI/AISI S400.

^oAlternately, the seismic load effect including overstrength, E_{mh} , is permitted to be based on the expected strength determined in accordance with ANSI/AISI S400. ^pOrdinary moment frame is permitted to be used in lieu of intermediate moment frame for Seismic Design Categories B or C.

Step 6: Establish Diaphragm behavior and Modelings requirements. Section 12:3.1 Diaphragm Flexibility - Flexible diaphragm conditions

Rigid diaphram condition -Calculated flexible diaphragm condition equivalent Static Loads If SMDD > 2 > Flexible

Step 7: Determine Configuration Irregularities.

Horizontal Structural irregularities -> Table 12.3-1

Vertical Structural irregularities -> Table 12.3-2

A ADVE

12.3 DIAPHRAGM FLEXIBILITY, CONFIGURATION IRREGULARITIES, AND REDUNDANCY

- **12.3.1 Diaphragm Flexibility.** The structural analysis shall consider the relative stiffnesses of diaphragms and the vertical elements of the seismic force-resisting system. Unless a diaphragm can be idealized as either flexible or rigid in accordance with Sections 12.3.1.1, 12.3.1.2, or 12.3.1.3, the structural analysis shall explicitly include consideration of the stiffness of the diaphragm (i.e., semirigid modeling assumption).
- **12.3.1.1 Flexible Diaphragm Condition.** Diaphragms constructed of untopped steel decking or wood structural panels are permitted to be idealized as flexible if any of the following conditions exist:
 - a. In structures where the vertical elements are steel braced frames; steel and concrete composite braced frames; or concrete, masonry, steel, or steel and concrete composite shear walls.
 - b. In one- and two-family dwellings.
 - c. In structures of light-frame construction where all of the following conditions are met:
 - 1. Topping of concrete or similar materials is not placed over wood structural panel diaphragms except for non-structural topping no greater than 1 1/2 in. (38 mm) thick.
 - 2. Each line of vertical elements of the seismic force-resisting system complies with the allowable story drift of Table 12.12-1.

12.3.1.2 Rigid Diaphragm Condition. Diaphragms of concrete slabs or concrete-filled metal deck with span-to-depth ratios of 3 or less in structures that have no horizontal irregularities are permitted to be idealized as rigid.

12.3.1.3 Calculated Flexible Diaphragm Condition. Diaphragms not satisfying the conditions of Sections 12.3.1.1 or 12.3.1.2 are permitted to be idealized as flexible provided:

$$\frac{\delta_{\text{MDD}}}{\Delta_{\text{ADVE}}} > 2 \tag{12.3-1}$$

where δ_{MDD} and Δ_{ADVE} are as shown in Fig. 12.3-1. The loading used in this calculation shall be that prescribed in Section 12.8.

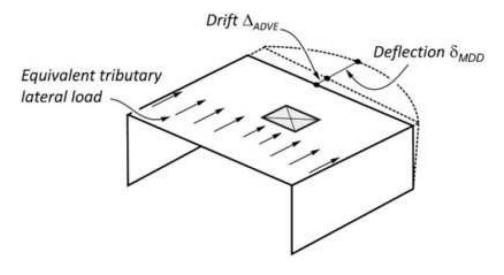


FIGURE 12.3-1 Flexible Diaphragm

Horizontal Irregularities

Table 12.3-1 Horizontal Structural Irregularities

| Туре | Description | Reference Section | Seismic Design Category Application |
|------|--|---|---|
| la. | Torsional Irregularity: Torsional irregularity is defined to exist where the maximum story drift, computed including accidental torsion with $A_x = 1.0$, at one end of the structure transverse to an axis is more than 1.2 times the average of the story drifts at the two ends of the structure. Torsional irregularity requirements in the reference sections apply only to structures in which the diaphragms are rigid or semirigid. | 12.3.3.4 12.7.3 12.8.4.3 12.12.1 Table 12.6-1 16.3.4 | D, E, and F B, C, D, E, and F C, D, E, and F C, D, E, and F D, E, and F B, C, D, E, and F |
| 1b. | Extreme Torsional Irregularity: Extreme torsional irregularity is defined to exist where the maximum story drift, computed including accidental torsion with $A_x = 1.0$, at one end of the structure transverse to an axis is more than 1.4 times the average of the story drifts at the two ends of the structure. Extreme torsional irregularity requirements in the reference sections apply only to structures in which the diaphragms are rigid or semirigid. | 12.3.3.1 12.3.3.4 12.3.4.2 12.7.3 12.8.4.3 12.12.1 Table 12.6-1 16.3.4 | E and F D D B, C, and D C and D C and D D B, C, and D |
| 2. | Reentrant Corner Irregularity: Reentrant corner irregularity is defined to exist where both plan projections of the structure beyond a reentrant corner are greater than 15% of the plan dimension of the structure in the given direction. | 12.3.3.4 Table 12.6-1 | D, E, and F D, E, and F |
| 3. | Diaphragm Discontinuity Irregularity: Diaphragm discontinuity irregularity is defined to exist where there is a diaphragm with an abrupt discontinuity or variation in stiffness, including one that has a cutout or open area greater than 50% of the gross enclosed diaphragm area, or a change in effective diaphragm stiffness of more than 50% from one story to the next. | 12.3.3.4 Table 12.6-1 | D, E, and F D, E, and F |
| 4. | Out-of-Plane Offset Irregularity: Out-of-plane offset irregularity is defined to exist where there is a discontinuity in a lateral force-resistance path, such as an out-of-plane offset of at least one of the vertical elements. | 12.3.3.3 12.3.3.4 12.7.3 Table 12.6-1 16.3.4 | B, C, D, E, and F D, E, and F B, C, D, E, and F D, E, and F B, C, D, E, and F |
| 5. | Nonparallel System Irregularity: Nonparallel system irregularity is defined to exist where vertical lateral force-resisting elements are not parallel to the major orthogonal axes of the seismic force-resisting system. | 12.5.3 12.7.3 Table 12.6-1 16.3.4 | C, D, E, and F B, C, D, E, and F D, E, and F B, C, D, E, and F |

Vertical Irregularities

Table 12.3-2 Vertical Structural Irregularities

| Туре | Description | Reference Section | Seismic Design Category Application |
|------|---|--------------------------------------|---|
| 1a. | Stiffness–Soft Story Irregularity: Stiffness–soft story irregularity is defined to exist where there is a story in which the lateral stiffness is less than 70% of that in the story above or less than 80% of the average stiffness of the three stories above. | Table 12.6-1 | D, E, and F |
| 1b. | Stiffness–Extreme Soft Story Irregularity: Stiffness–extreme soft story irregularity is defined to exist where there is a story in which the lateral stiffness is less than 60% of that in the story above or less than 70% of the average stiffness of the three stories above. | 12.3.3.1 Table 12.6-1 | E and F D, E, and F |
| 2. | Weight (Mass) Irregularity: Weight (mass) irregularity is defined to exist where the effective mass of any story is more than 150% of the effective mass of an adjacent story. A roof that is lighter than the floor below need not be considered. | Table 12.6-1 | D, E, and F |
| 3. | Vertical Geometric Irregularity: Vertical geometric irregularity is defined to exist where the horizontal dimension of the seismic force-resisting system in any story is more than 130% of that in an adjacent story. | Table 12.6-1 | D, E, and F |
| 4. | In-Plane Discontinuity in Vertical Lateral Force-Resisting Element Irregularity: In-plane discontinuity in vertical lateral force-resisting element irregularity is defined to exist where there is an in-plane offset of a vertical seismic force-resisting element resulting in overturning demands on supporting structural elements. | 12.3.3.3 12.3.3.4 Table 12.6-1 | B, C, D, E, and F D, E, and F D, E, and F |
| 5a. | Discontinuity in Lateral Strength–Weak Story Irregularity: Discontinuity in lateral strength–weak story irregularity is defined to exist where the story lateral strength is less than 80% of that in the story above. The story lateral strength is the total lateral strength of all seismic-resisting elements sharing the story shear for the direction under consideration. | 12.3.3.1 Table 12.6-1 | E and F D, E, and F |
| 5b. | Discontinuity in Lateral Strength–Extreme Weak Story Irregularity: Discontinuity in lateral strength–extreme weak story irregularity is defined to exist where the story lateral strength is less than 65% of that in the story above. The story strength is the total strength of all seismic-resisting elements sharing the story shear for the direction under consideration. | 12.3.3.1 12.3.3.2 Table 12.6-1 | D, E, and F B and C D, E, and F |

Step 8: Selection of Method of Analysis.

Based on SDC and Structural characteristics

e.g. height and irregularities, check the permitted

analysis procedures using Table 12.6-1 [ASCE 7-16]

Table 12.6-1 Permitted Analytical Procedures

| Seismic Design Category | Structural Characteristics | Equivalent Lateral Force Procedure, Section 12.8 ^a | Modal Response Spectrum Analysis, Section 12.9.1, or Linear Response History Analysis, Section 12.9.2 ^a | Nonlinear Response History Procedures, Chapter 16 ^a |
|-------------------------------|---|---|---|--|
| В, С | All structures | P | P | Р |
| D, E, F | Risk Category I or II buildings not exceeding two stories above the base | P | P | P |
| | Structures of light-frame construction | P | P | P |
| | Structures with no structural irregularities and not exceeding 160 ft (48.8 m) in structural height | P | P | P |
| | Structures exceeding 160 ft (48.8 m) in structural height with no structural irregularities and with $T < 3.5T_s$ | P | P | P |
| | Structures not exceeding 160 ft (48.8 m) in structural height and having only horizontal irregularities of Type 2, 3, 4, or 5 in Table 12.3-1 or vertical irregularities of Type 4, 5a, or 5b in Table 12.3-2 | P | P | P |
| | All other structures | NP | P | P |

^aP: Permitted; NP: Not Permitted; $T_s = S_{D1}/S_{DS}$.

Modelling Criteria

```
· Foundation -> Fix Support or Consider foundation
                                                     flexibility
                                                     (Ch 19, ASCE7)
· Effective Seismic Weight = (W)
                                  + 0.25 live [except if storage
                                                 loads > W]
                                                [except public garages,
                                   + partition walls [or 10 psf of floor
                                                    area whichever is
                                   + permanent greater]
equipment
                                   +0.2 Snow [if flat 800f snow load > 30 psf]
                                    + Land scaping / roof gardens.
```

Modelling Criteria

- · Concrete and masonry elements -> Stiffness properties of Cracked Sections.
- · Steel MRFs -> Contribution of panel zone deformations to overall story drift shall be included.
- . Horizontal Irregularity type 19, 16, 4 or 5 (Table 12.3-1)
- In 3D Model, minimum three dynamic DOFS at each floor.

 Z

 UX, UY, RZ

• P∆ effects should not be included directly in the analysis,

they are considered indirectly in section 12.8.7.

The analysis results will be used to check faccount for PD.

Modelling Criteria

- · Floor diaphragms -> Shell elements
- · Flexural, shear, Axial and Torsional deformations -> include in all beams and Columns -> 3D Frame elements.
- · Beam-column joints -> Centerline dimensions Ly Approximately accounts for
- · Basement walls -> Shell element. L> Basement may act as a very stiff first

floox.

Thank you for your attention