# Probabilistic Ground Motions in Earthquake-resistant Design of Buildings





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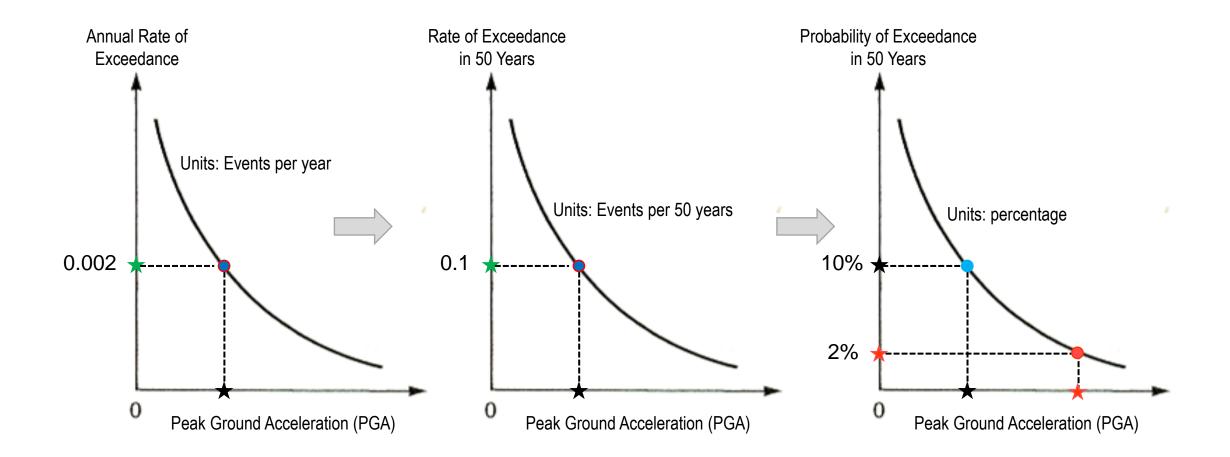
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# Use of Probabilistic Ground Motions in Earthquake-resistant Design of Buildings

Performance-based Seismic Design of Buildings – Semester: Spring 2020 (Fawad A. Najam)

### **Different Forms of Hazard Curves**

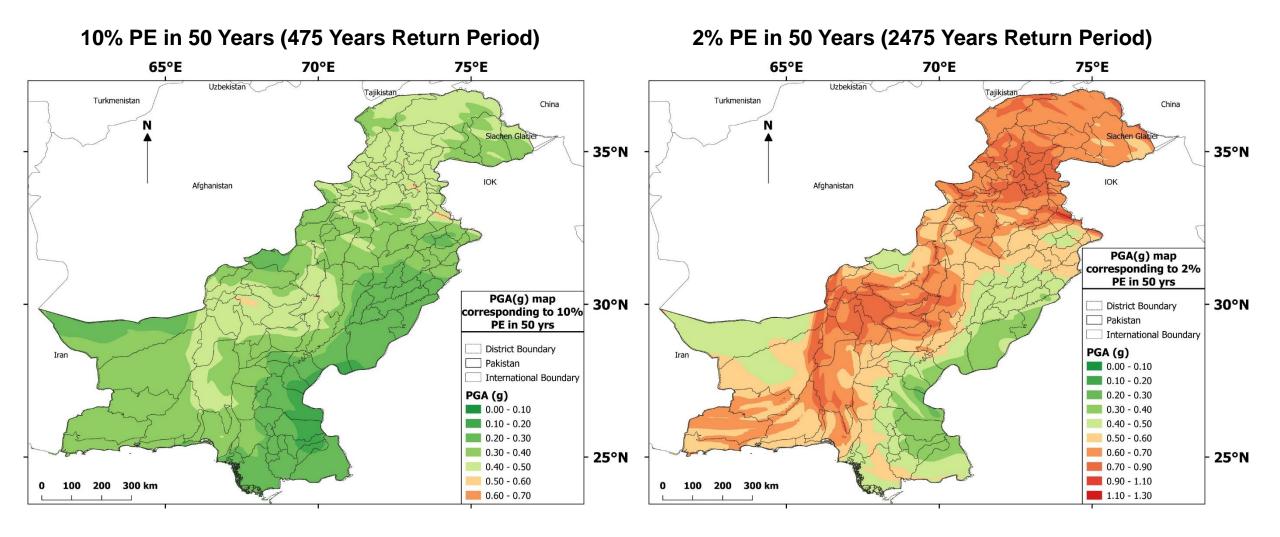


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### Probabilistic Seismic Hazard Analysis

### Seismic Hazard Map of Pakistan



### Use of Probabilistic Ground Motions in Earthquake-resistant Design of Buildings

- The expected performance of buildings in modern earthquake-resistant design codes are:
  - 1) Resist a minor level of earthquake ground shaking (SE) without damage SE = Serviceability earthquake—50% probability of exceedance in 30 years (43-year return period)
  - Resist the design level of earthquake ground shaking (DBE) with damage (which may or may not be economically repaired) but without causing extensive loss of life.
     DBE = Design basis earthquake—10% probability of exceedance in 50 years (475-year return period)
  - 3) Resist **the strongest earthquake** shaking expected at the site (MCE) without collapse, but potentially with extreme damage.

*MCE* = *Maximum* considered earthquake—2% probability of exceedance in 50 years (2475-year return period)

## **Seismic Design Criteria of Major Dam Projects**

- According to ICOLD (International Commission of Large Dams) Bulletin 72 (1989), large dams have to be able to withstand the effects of the Maximum Credible Earthquake Shaking Level (MCE).
- This MCE is the strongest earthquake shaking level that could occur in the region of a dam, and is considered to have a return period of several thousand years (typically 10,000 years in regions of low to moderate seismicity).

MCE = Maximum considered earthquake—0.5% probability of exceedance in 50 years (about 10,000-year return period)

## Probabilistic Ground Motion Parameters: PGA, PGV, SA

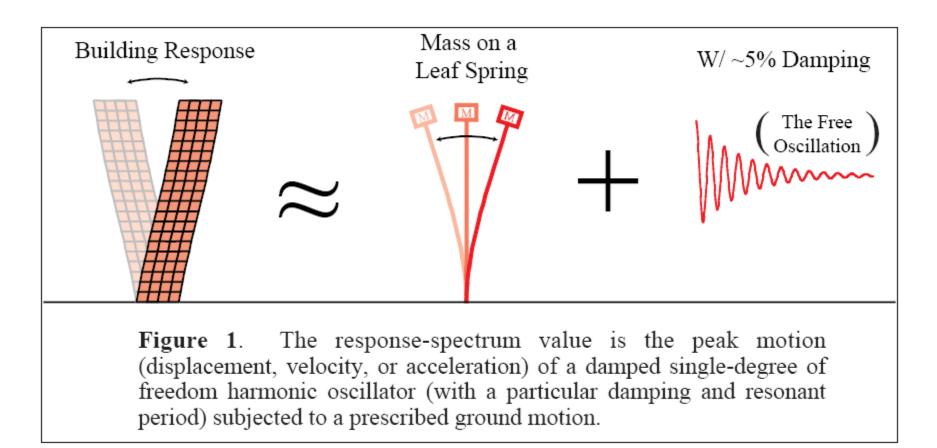
- Traditionally Peak Ground Acceleration (PGA) has been used to quantify ground motion in PSHA. PGA is a good index to hazard for low-rise buildings, up to about 7 stories.
- **PGV**, **peak ground velocity**, is a good index to hazard to taller buildings. However, it is not clear how to relate velocity to force in order to design a taller building.
- Today the preferred parameter is **Response Spectral Acceleration (SA)**.
- While PGA (peak acceleration) is what is experienced by a particle on the ground, SA is approximately what is experienced by a building, as modeled by a particle mass on a massless vertical rod having the same natural period of vibration as the building.

SA = The maximum acceleration experienced by a damped, single-degree-of-freedom oscillator (a crude representation of building response).

Max. Earthquake Force in the Building = Building Mass x SA

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### **Response Spectrum Parameters: SA, SD, SV**



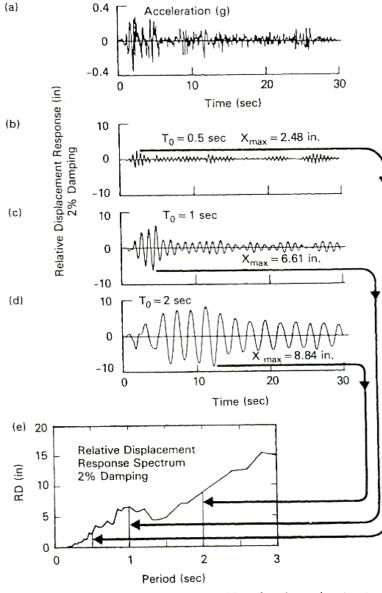
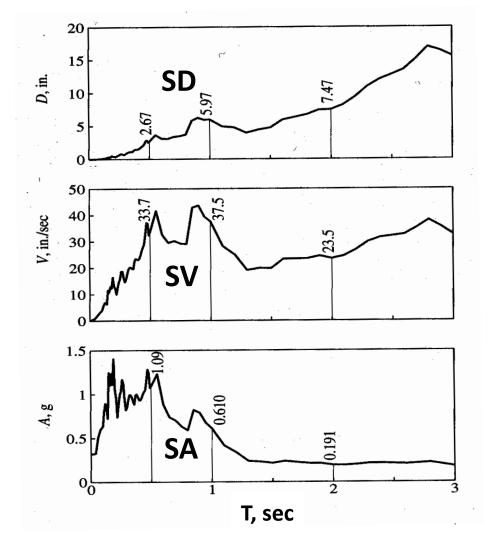


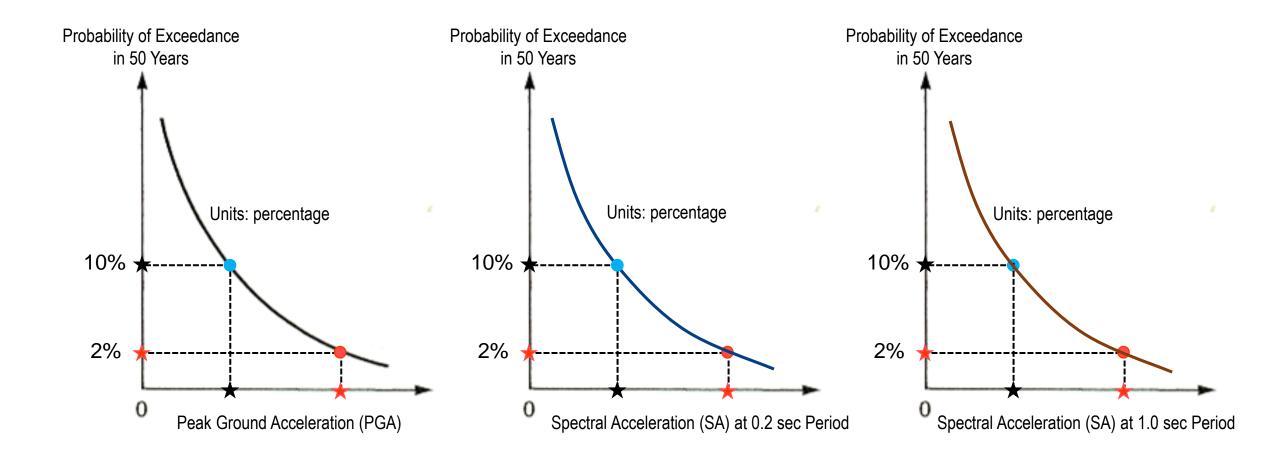
FIGURE 6.3 Construction of a response spectrum. (a) earthquake acceleration time history (El Centro, California 1940) used as input, (b) relative displacement response of a 2% damped oscillator with a natural period of 0.5 seconds, (c) relative displacement response of a 2% damped oscillator with a natural period of 1.0 seconds, (d) relative displacement response of a 2% damped oscillator with a natural period of 2.0 seconds and (e) maxima of b, c and d become points on the 2% damped relative displacement response spectrum (after Chopra 1981).

If we look at the displacement response, we can identify the maximum displacement. If we take the derivative (rate of change) of the displacement response with respect to time, we can get the velocity response. The maximum velocity can likewise be determined. Similarly for response acceleration (rate of change of velocity) also called response spectral acceleration (SA).



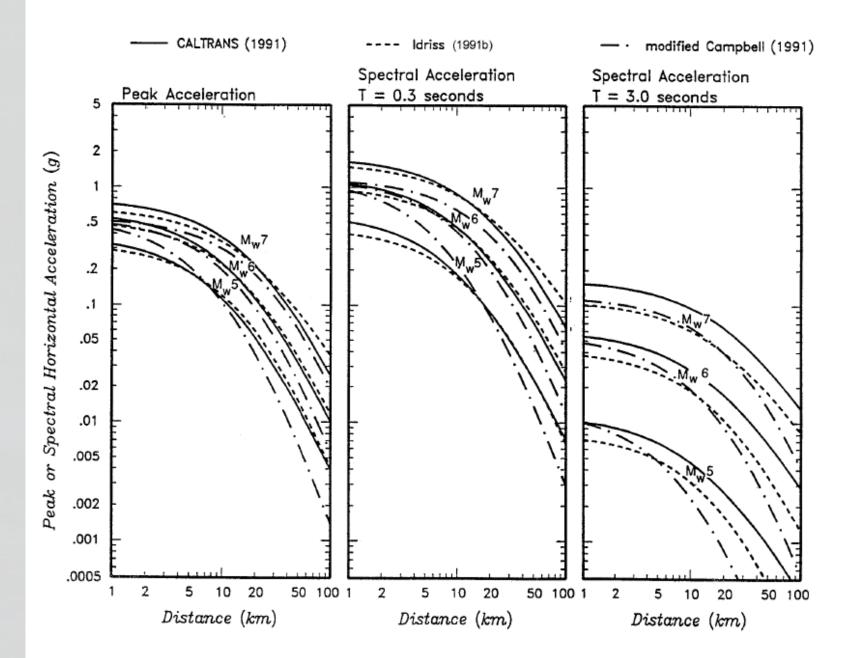
**Construction of Response Spectra (for Past Earthquakes**)

### **Hazard Curves for Spectral Acceleration**



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### **Attenuation Model for SA**



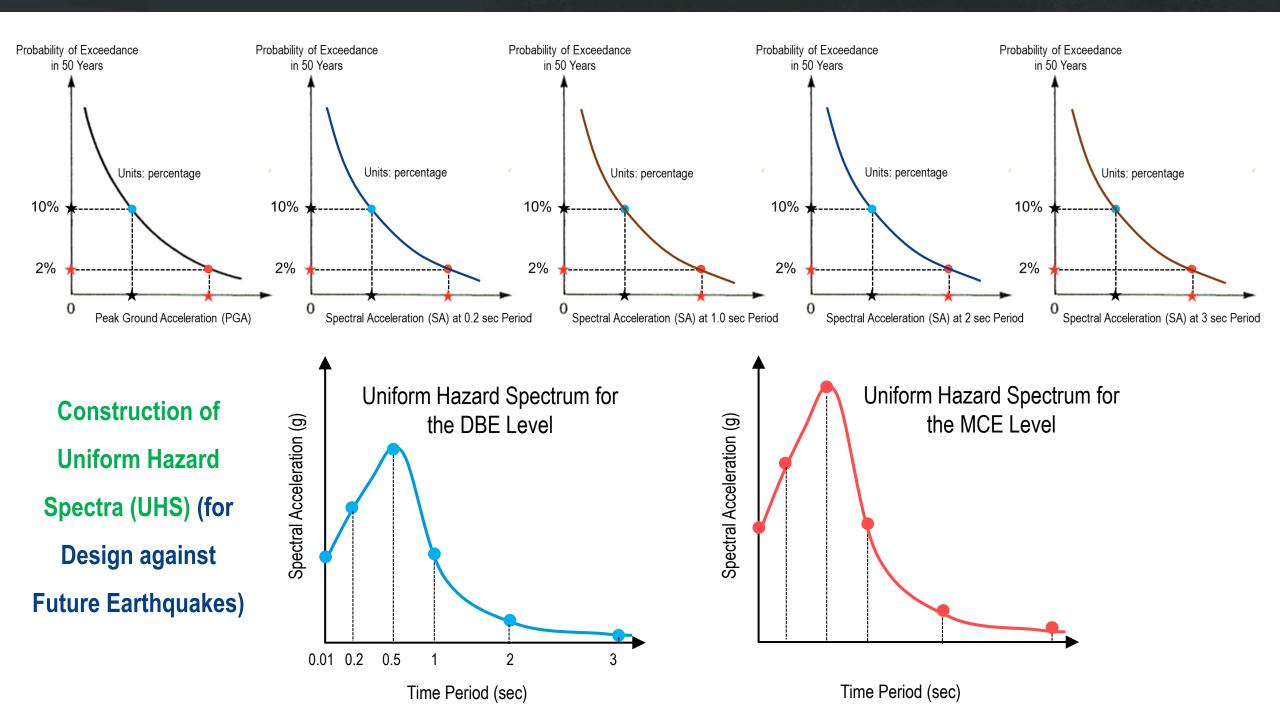
### **Coefficients of an attenuation relationship**

$T_n(\mathbf{s})$	<i>c</i> <sub>1</sub>	<i>c</i> <sub>2</sub>	C3	$c_4$	<i>C</i> <sub>5</sub>	c <sub>6</sub>	<i>c</i> <sub>7</sub>	C <sub>8</sub>	С <sub>9</sub>	<i>c</i> <sub>10</sub>	<i>c</i> <sub>11</sub>	<i>c</i> <sub>12</sub>	<i>c</i> <sub>13</sub>	C <sub>14</sub>
						$M_W \le 0$	5.5							
PGA	0.182	-0.624	1.0	0	-2.100	0	3.6564	0.250	0	1.39	0.14	0.38	0	7.2
0.05	0.182	-0.090	1.0	0.006	-2.128	-0.082	3.6564	0.250	0	1.39	0.14	0.38	0	7.2
0.07	0.182	0.110	1.0	0.006	-2.128	-0.082	3.6564	0.250	0	1.40	0.14	0.39	0	7.2
0.09	0.182	0.212	1.0	0.006	-2.140	-0.052	3.6564	0.250	0	1.40	0.14	0.39	0	7.2
0.10	0.182	0.275	1.0	0.006	-2.148	-0.041	3.6564	0.250	0	1.41	0.14	0.40	0	7.2
0.12	0.182	0.348	1.0	0.005	-2.162	-0.014	3.6564	0.250	0	1.41	0.14	0.40	0	7.2
0.14	0.182	0.307	1.0	0.004	-2.144	0	3.6564	0.250	0	1.42	0.14	0.41	0	7.2
0.15	0.182	0.285	1.0	0.002	-2.130	0	3.6564	0.250	0	1.42	0.14	0.41	0	7.2
0.17	0.182	0.239	1.0	0	-2.110	0	3.6564	0.250	0	1.42	0.14	0.41	0	7.2
0.20	0.182	0.153	1.0	-0.004	-2.080	0	3.6564	0.250	0	1.43	0.14	0.42	0	7.2
0.24	0.182	0.060	1.0	-0.011	-2.053	0	3.6564	0.250	0	1.44	0.14	0.43	0	7.2
0.30	0.182	-0.057	1.0	-0.017	-2.028	0	3.6564	0.250	0	1.45	0.14	0.44	0	7.2
0.40	0.182	-0.298	1.0	-0.028	-1.990	0	3.6564	0.250	0	1.48	0.14	0.47	0	7.2
0.50	0.182	-0.588	1.0	-0.040	-1.945	0	3.6564	0.250	0	1.50	0.14	0.49	0	7.2
0.75	0.182	-1.208	1.0	-0.050	-1.865	0	3.6564	0.250	0	1.52	0.14	0.51	0	7.2
1.0	0.182	-1.705	1.0	-0.055	-1.800	0	3.6564	0.250	0	1.53	0.14	0.52	0	7.2
1.5	0.182	-2.407	1.0	-0.065	-1.725	0	3.6564	0.250	0	1.53	0.14	0.52	0	7.2
2.0	0.182	-2.945	1.0	-0.070	-1.670	0	3.6564	0.250	0	1.53	0.14	0.52	0	7.2
3.0	0.182	-3.700	1.0	-0.080	-1.610	0	3.6564	0.250	0	1.53	0.14	0.52	0	7.2
4.0	0.182	-4.230	1.0	-0.100	-1.570	0	3.6564	0.250	0	1.53	0.14	0.52	0	7.2
5.0	0.182	-4.714	1.0	-0.100	-1.540	0	3.6564	0.250	0	1.53	0.14	0.52	0	7.
7.5	0.182	-5.530	1.0	-0.110	-1.510	0	3.6564	0.250	0	1.53	0.14	0.52	0	7.

TABLE 5.11 Coefficients for Sadigh et al. Rock Attenuation Relation: Horizontal Component

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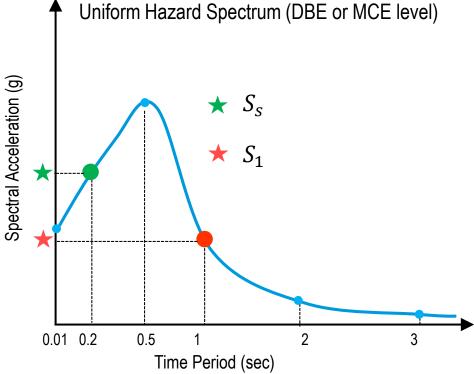
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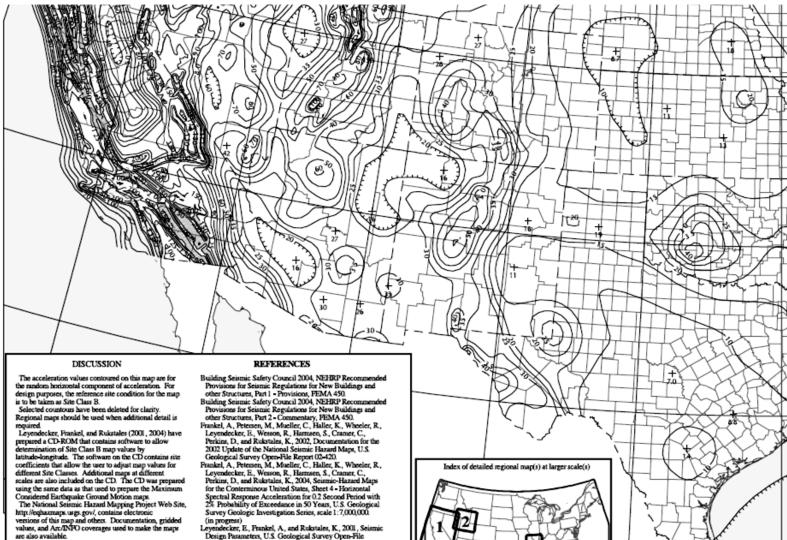
## $S_s$ and $S_1$ in Building Codes

- $S_s$  = Short-period Spectral Acceleration
  - = SA (0.2 sec Time Period)

- $S_1$  = Short-period Spectral Acceleration
  - = SA (1.0 sec Time Period)



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are also available. The California portion of the map was produced jointly with the California Geological Survey.

Map prepared by U.S. Geological Survey.

Report 01-437. Leyendecker, E., Frankel, A., and Rukstales, K., 2004, Seismic Design Parameters, U.S. Geological Survey Open-File Report (in progress) National Seismic Hazard Mapping Project Web Site, http://eqhazmaps.usgs.gov, U. S. Geological Survey.

- Region 1 is shown enlarged in figure 22-3 - Region 2 is shown enlarged in figure 22-5 - Region 3 is shown enlarged in figure 22-7 - Region 4 is shown enlarged in figure 22-9

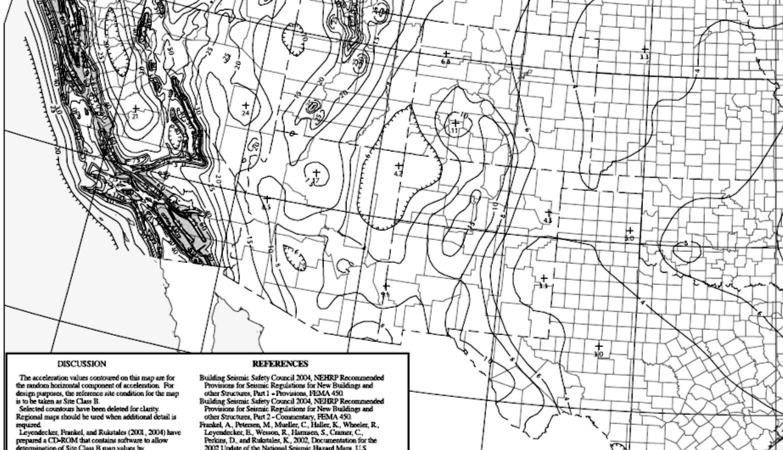
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M

100°

95°

FIGURE 22-1 MAXIMUM CONSIDERED EARTHQUAKE GROUND MOTION FOR THE CONTERMINOUS UNITED STATES OF 0.2 SEC SPECTRAL RESPONSE ACCELERATION (5% OF CRITICAL DAMPING), SITE CLASS B



determination of Site Class B map values by latitude-longitude. The software on the CD contains site coefficients that allow the user to adjust map values for different Site Classes. Additional maps at different scales are also included on the CD. The CD was prepared scales are also included on the C.D. The C.D was prepared using the same data as that used to prepare the Maximum Considered Earthquake Ground Morion maps. The National Sesimic Harard Mapping Project Web Site, http://eqhazmaps.usg.gov/, contains electronic versions of this map and others. Documentation, gidded values, and Arc.INRO coverages used to make the maps are also available.

The California portion of the map was produced jointly with the California Geological Survey.

Map prepared by U.S. Geological Survey.

2002 Update of the National Seismic Hazard Maps, U.S. 2022 Optime of the Valuentia Seature Fatzard Wags, U.S. Geological Survey Oper-Hic Report (02-420, Frankel, A., Petersen, M., Maeller, C., Haller, K., Wheeler, R., Leyendecker, E., Wesson, R., Harmsen, S., Cramer, C., Perfins, D., and Rukralack, K., 2004, Scinnio-Hazard Maps for the Conterminous United States, Sheet 6-Horizontal Spectral Response Acceleration for 1.0 Second Period with 2% Probability of Exceedance in 50 Years, U.S. Geological Survey Geologic Investigation Series, scale 1:7,000,000

(in progress). Leyendecker, E., Frankel, A., and Rukstales, K., 2001, Seismic Design Parameters, U.S. Geological Survey Open-File Report 01-437.

Leyendecker, E., Frankel, A., and Rukstales, K., 2004, Seismic Design Parameters, U.S. Geological Survey Open-File

Report (in progress). National Seismic Hazard Mapping Project Web Site, http://eqhazmaps.usgs.gov, U. S. Geological Survey.

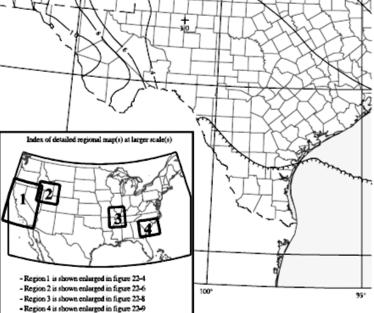
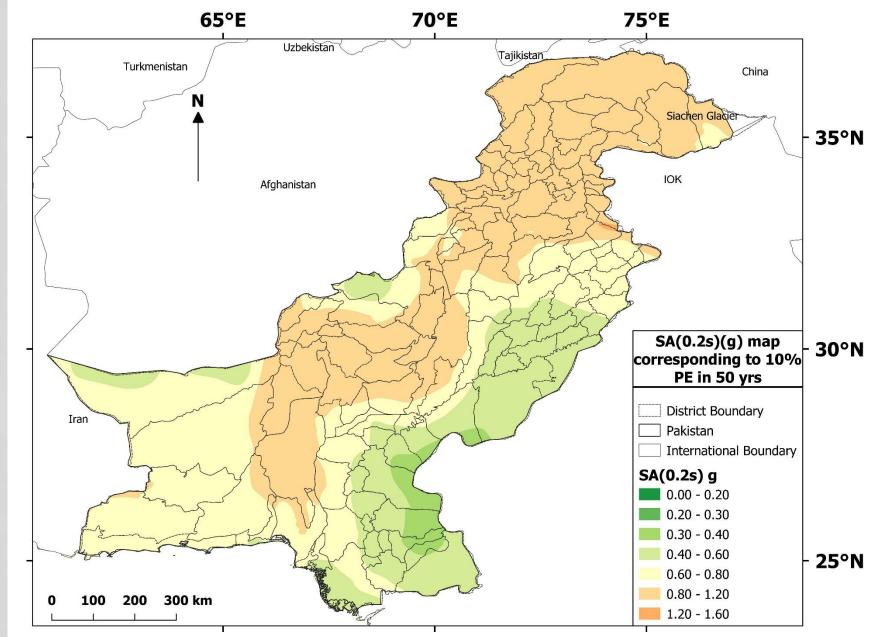
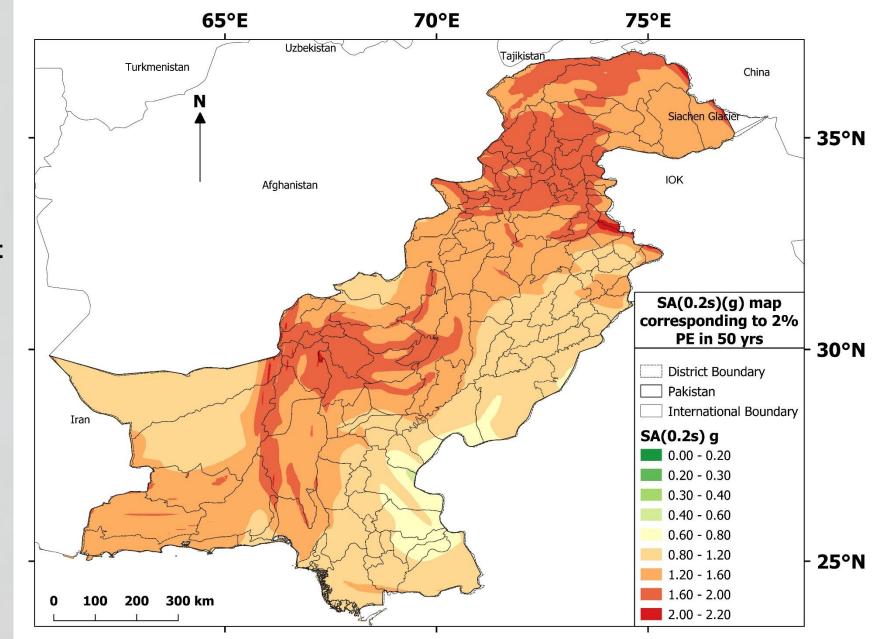


FIGURE 22-2 MAXIMUM CONSIDERED EARTHQUAKE GROUND MOTION FOR THE CONTERMINOUS UNITED STATES OF 1.0 SEC SPECTRAL RESPONSE ACCELERATION (5% OF CRITICAL DAMPING), SITE CLASS B

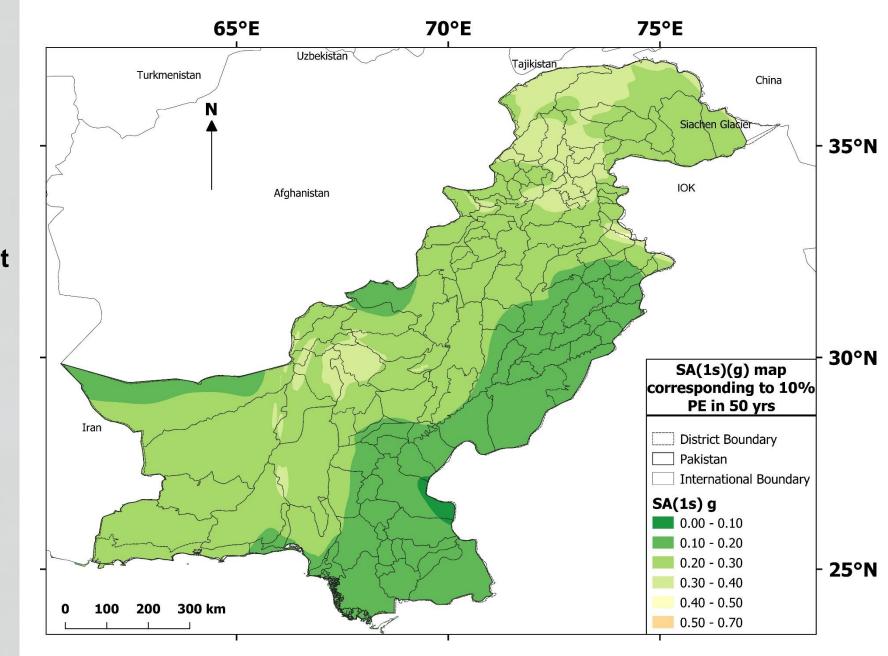
Spectral Acceleration (SA) at 0.2 sec. map for 475 years RP (10% PE in 50 years)



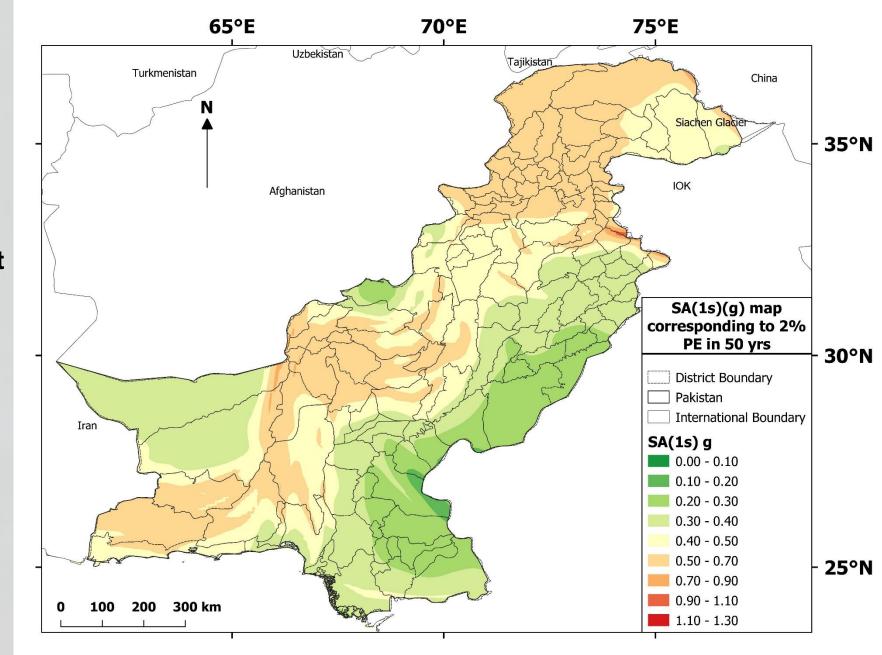
Spectral Acceleration (SA) at 0.2 sec. map for 2475 years RP (2% PE in 50 years)



Spectral Acceleration (SA) at 1.0 sec. map for 475 years RP (10% PE in 50 years)



Spectral Acceleration (SA) at 1.0 sec. map for 2475 years RP (2% PE in 50 years)



## **Deaggregation of Seismic Hazard**

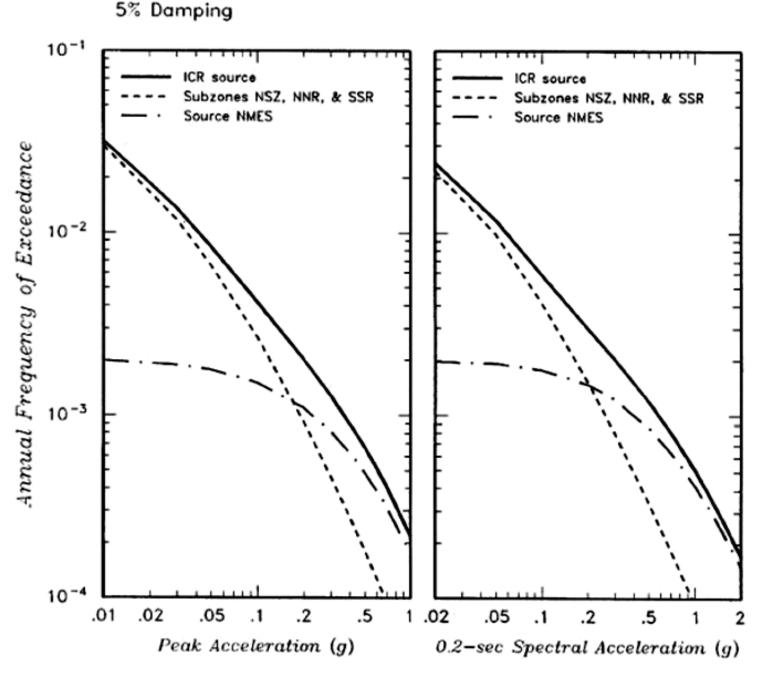
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## **Deaggregation of Seismic Hazard**

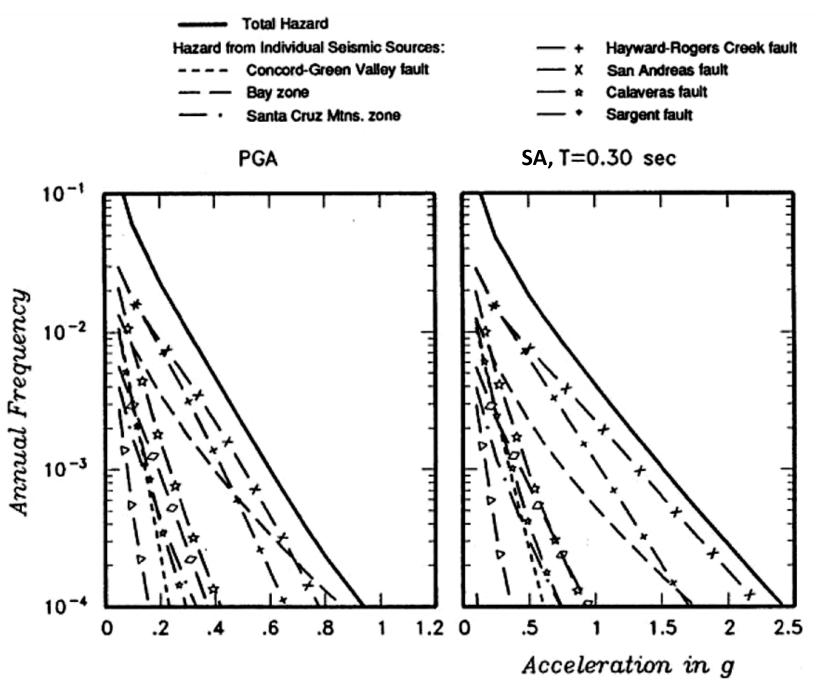
- The hazard curve gives the **combined effect** of all the seismic sources, magnitudes and distances on the probability of exceeding a given ground motion level.
- Since all of the sources, magnitudes, and distances are mixed together, it is difficult to get an intuitive understanding of what is controlling the hazard from the hazard curve by itself.
- To provide insight into what events are the most important for the hazard at a given ground motion level, the hazard curve is broken down into its contributions from different earthquake scenarios.

• This process is called 'Deaggregation of Hazard'.

Example of Contributions of Various Seismic Sources to the Total Seismic Hazard at the Site



Example of Contributions of Various Seismic Sources to the Total Seismic Hazard at the Site



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### Example of Contributions of Various Seismic Sources to the Total Seismic Hazard at the Site

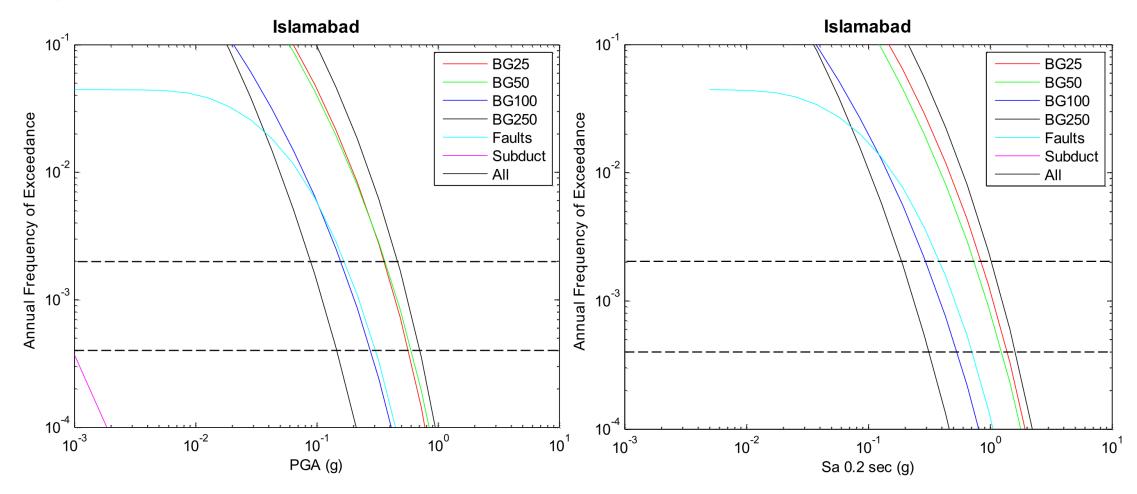
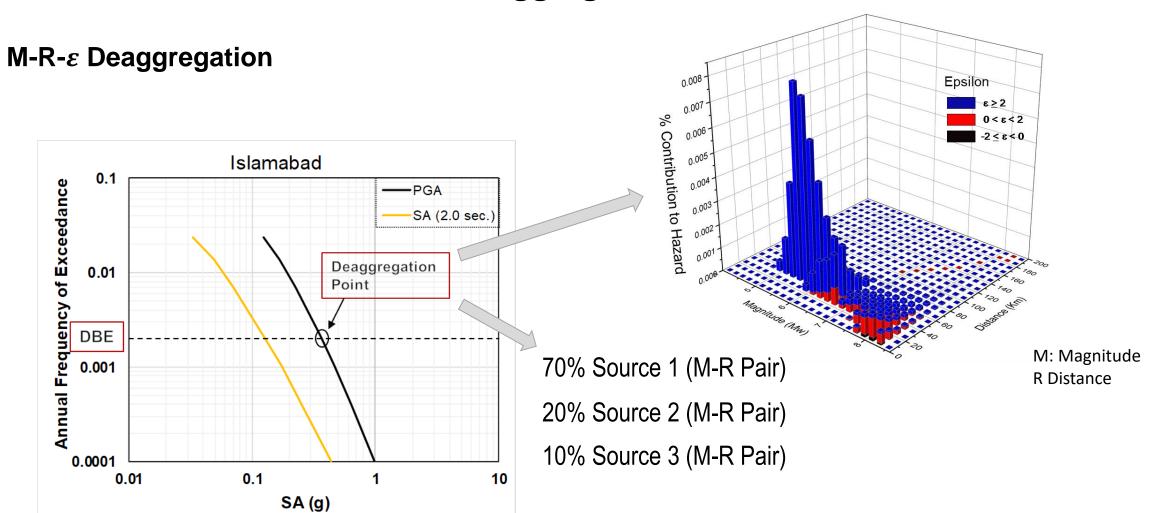


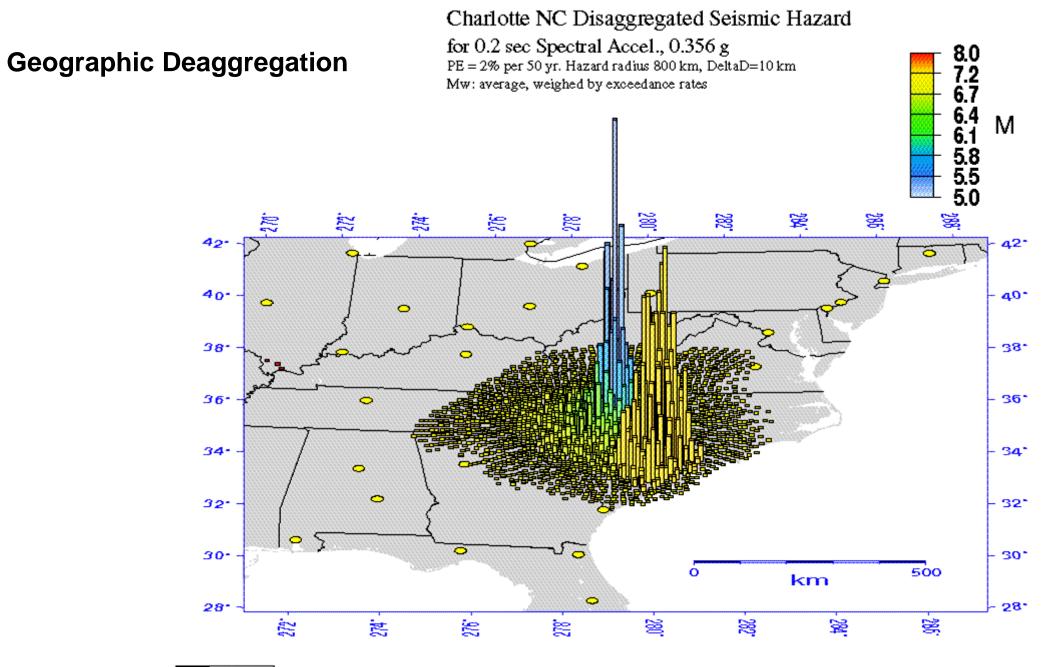
Figure. 3.17 (a) Seismic hazard curves for PGA and 0.2-second SA for Islamabad and contributions of six different earthquake sources to the hazard (BG25: Background shallow seismicity (0-25 km), (BG50: Background shallow seismicity (25-50km), BG100: Background intermediate depth seismicity (50-100 km), BG250: Background deep seismicity (100-250 km), Faults, Makran Subduction zone (Subduct) and All Source (All)).

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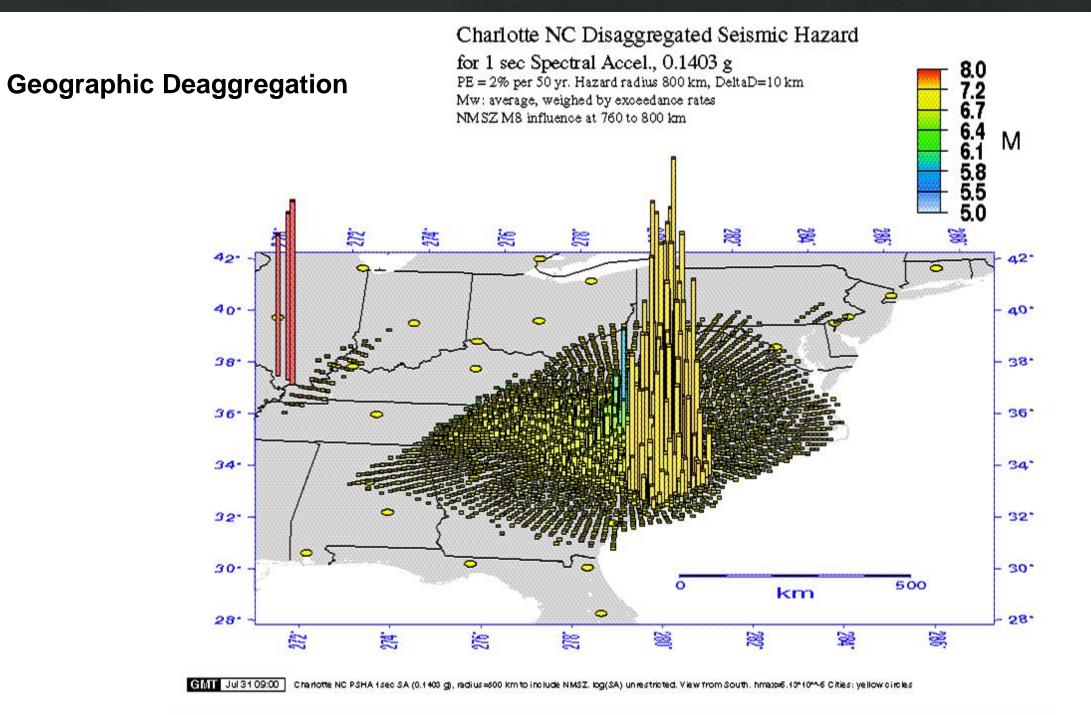


## **Probabilistic Seismic Hazard Deaggregation**

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### Charlotte NC PSHA 0.2 sec SA (0.356 g), radius=800 km to include NMSZ. log(SA) unrestricted. View from South. hmax=8.63\*10\*\*6 Cities: yellow circles



### **Deaggregation of Seismic Hazard at Islamabad (Pakistan)**

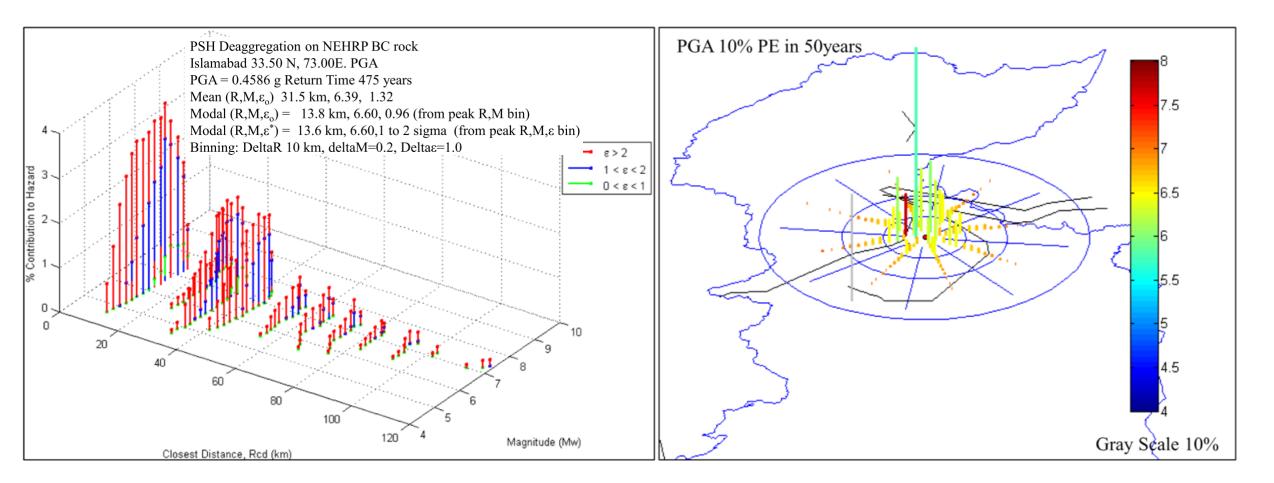


Figure 4.3 Deaggregation plots for Islamabad. PGA (10% PE in 50years): M-R- $\varepsilon_0$  (left) and Geographic (right). The red dot and black line in Geographic Plot shows the location of Islamabad and crustal faults, respectively.

Source: Zaman (2016)

		SA (g)		Mean			Modal	
Site	T (s)	at 475- years	Μ	R (km)	<b>E</b> 0	Μ	R (km)	<b>E</b> 0
	0	0.4586	6.39	31.5	1.32	6.6	13.8	0.96
Islamabad	0.2	1.0214	6.41	28.0	1.36	6.6	14.1	0.83
Islamavau	1.0	0.2691	6.91	37.4	1.29	7.78	23.6	0.88
	2.0	0.1096	7.08	42.0	1.24	7.79	23.6	0.54
	0	0.3908	6.56	51.6	1.26	6.80	44.6	0.57
Peshawar	0.2	0.8160	6.59	32.5	1.31	7.78	32.5	1.09
resnawar	1	0.2283	7.01	68.8	1.34	7.65	32.5	0.85
	2	0.0938	7.10	81.7	1.36	7.78	32.5	0.45
	0	0.4548	6.45	34.7	1.28	6.6	35.2	0.71
Quatta	0.2	0.9923	6.46	31.6	1.34	6.6	14.2	0.81
Quetta	1	0.2602	6.94	36.9	1.25	7.44	23.2	1.14
	2	0.1090	7.19	55.8	1.16	7.57	22.8	0.7
	0	0.2918	6.43	53.2	1	5.8	37.2	0.99
Karachi	0.2	0.6141	6.56	56.7	1.14	5.8	37.1	1.12
Naraciii	1	0.1778	7.25	92.9	1.25	8.11	122.1	0.76
	2	0.0792	7.51	145	1.35	8.11	125.5	0.76

### Table 4.1 Mean and Modal values of M-R- $\varepsilon_o$ for 10% PE in 50-years

### Mean and Modal values of

### **M-R-***ε* for 10% PE in 50-

years

Source: Zaman (2016)

		SA (g) at		Mean		Modal			
Site	T (s)	2475-years	Μ	R (km)	<b>E</b> 0	Μ	R (km)	<b>E</b> 0	
	0	0.7092	6.58	29.9	1.68	6.6	13	1.61	
Islamabad	0.2	1.6212	6.58	25.5	1.74	6.6	13.3	1.5	
15141114044	1	0.4413	7.01	28.3	1.66	6.8	13.7	1.35	
	2	0.1880	7.19	30.5	1.60	7.77	23.6	1.36	
	0	0.6206	6.74	45.8	1.58	7.00	35.4	0.75	
Peshawar	0.2	1.3194	6.75	43	1.63	7.00	35.2	0.95	
1 0511 a Wal	1	0.3781	7.14	52.6	1.70	7.65	32.5	1.63	
	2	0.1629	7.26	58.2	1.64	7.81	32.5	1.26	
	0	0.706	6.63	33.3	1.63	7.2	35.3	0.72	
Quetta	0.2	1.5795	6.62	29.4	1.71	6.6	13.4	1.47	
Queila	1	0.4295	7.02	29.9	1.69	7.45	23.2	1.92	
	2	0.1903	7.26	37	1.63	7.59	22.8	1.47	
	0	0.4978	6.62	46.1	1.29	6.6	35.6	0.83	
Karachi	0.2	1.0652	6.71	48.9	1.43	6.6	35.4	0.95	
ixai aviii	1	0.3082	7.36	81.5	1.62	8.04	118.6	1.72	
	2	0.1385	7.61	126.5	1.73	8.09	122.5	1.70	

Table 4.2 Mean and Modal values of M-R- $\varepsilon_o$  for 2% PE in 50-years

### Mean and Modal values of

M-R- $\varepsilon$  for 2% PE in 50-

years

Source: Zaman (2016)

Contribution from individual seismic sources to Islamabad (10% PE in 50-years)

	PGA 10%	PE in 50-y	ears		
Details of principal seismic		ermediate &	t deep se	eismicity	, faults, subduction) if its
contribution to seismic haz Seismic Source	% Contribution	R [km]	Μ	1	Eps0 [mean values]
Shallow seismicity	92.03	29.9	6.32		1.28
Details of Individual fault	having seismic hazard	contributio			
ID & Fault Name	% Contribution	R [km]	Μ	Eps0	Site-to-source azimuth
				-	[degree (d)]
3, MBT Charac	3.89	29.9	7.78	1.53	-41.5
	0.2sec SA 10	% PE in 5(	)-years		
Details of principal seismic	c sources (shallow, inte	rmediate &	t deep se	sismicity	, faults, subduction) if its
contribution to seismic haz	zard >10%				
Seismic Source	% Contribution	R [km]	Μ	]	Eps0 [mean values]
Shallow seismicity	92.19	26.8	6.32		1.33
Crustal Faults	5.67	25.4	7.64		1.58
Details of Individual fault	having seismic hazard	contribution	n > 2%		
ID & Fault Name	% Contribution	R [km]	Μ	Eps0	Site to source agimuth
		IN [KIII]	1 V .		Site-to-source azimuth
		K [Kiii]		- <b>r</b> ~~	[d]

Table 4.3 Contribution from individual seismic sources to Islamabad (10% PE in 50-years)

### 1.0sec SA 10% PE in 50-years

Details of principal seismic sources (shallow, intermediate & deep seismicity, faults, subduction) if its contribution to seismic hazard >10%

Seismic Source	% Contribution	<b>R</b> [km]	Μ	]	Eps0 [mean values]
Shallow seismicity	73.59	33.4	6.72		1.25
<b>Crustal Faults</b>	20.61	33	7.60		1.28
Intermediate & Deep	5.80	103.6	6.95		1.84
seismicity (50 to 200 km)					
Details of Individual fault l	having seismic hazard	contribution	n > 2%		
ID & Fault Name	% Contribution	R (km)	Μ	Eps0	Site-to-source azimuth
				-	[d]
3, MBT Charac	13.37	23.6	7.79	0.89	-41.5
	2.0sec SA 10	% PE in 50	0-years		
	(1 11 · )	man adiata P	deen se	igminity	faulta aubduction) if ita
Details of principal seismic contribution to seismic haz			c ucep se	isincity	
1 1		R [km]	M	-	Eps0 [mean values]
contribution to seismic haz	ard >10%			-	,
contribution to seismic haz Seismic Source	ard >10% % Contribution	R [km]	M	-	Eps0 [mean values]
contribution to seismic haz Seismic Source Shallow seismicity	ard >10% % Contribution 58.13	<b>R [km]</b> 23.5	M 6.88	-	Eps0 [mean values] 1.58
contribution to seismic haz Seismic Source Shallow seismicity Crustal Faults Intermediate & Deep seismicity (50 to 200 km)	ard >10% % Contribution 58.13 35.18 6.69	<b>R [km]</b> 23.5 29.3 97.7	M 6.88 7.73 7.07	-	Eps0 [mean values] 1.58 1.53
contribution to seismic haz Seismic Source Shallow seismicity Crustal Faults Intermediate & Deep	ard >10% % Contribution 58.13 35.18 6.69	<b>R [km]</b> 23.5 29.3 97.7	M 6.88 7.73 7.07	-	Eps0 [mean values] 1.58 1.53
contribution to seismic haz Seismic Source Shallow seismicity Crustal Faults Intermediate & Deep seismicity (50 to 200 km)	ard >10% % Contribution 58.13 35.18 6.69	<b>R [km]</b> 23.5 29.3 97.7	M 6.88 7.73 7.07	-	Eps0 [mean values] 1.58 1.53
contribution to seismic haz Seismic Source Shallow seismicity Crustal Faults Intermediate & Deep seismicity (50 to 200 km) Details of Individual fault I	ard >10% % Contribution 58.13 35.18 6.69 having seismic hazard	<b>R [km]</b> 23.5 29.3 97.7 contribution	M     6.88     7.73     7.07     m > 2%	]	Eps0 [mean values] 1.58 1.53 2.13
contribution to seismic haz Seismic Source Shallow seismicity Crustal Faults Intermediate & Deep seismicity (50 to 200 km) Details of Individual fault I	ard >10% % Contribution 58.13 35.18 6.69 having seismic hazard	<b>R [km]</b> 23.5 29.3 97.7 contribution	M     6.88     7.73     7.07     m > 2%	]	Eps0 [mean values] 1.58 1.53 2.13 Site-to-source azimuth
contribution to seismic haz Seismic Source Shallow seismicity Crustal Faults Intermediate & Deep seismicity (50 to 200 km) Details of Individual fault I ID & Fault Name	ard >10% % Contribution 58.13 35.18 6.69 having seismic hazard % Contribution	<b>R [km]</b> 23.5 29.3 97.7 contribution <b>R (km)</b>	$     \begin{array}{r}         M \\         6.88 \\         7.73 \\         7.07 \\         \underline{n > 2\%} \\         M     \end{array} $	Eps0	Eps0 [mean values] 1.58 1.53 2.13 Site-to-source azimuth [d]
contribution to seismic haz Seismic Source Shallow seismicity Crustal Faults Intermediate & Deep seismicity (50 to 200 km) Details of Individual fault 1 ID & Fault Name 3, MBT Charac	ard >10% % Contribution 58.13 35.18 6.69 having seismic hazard % Contribution 18.80	<b>R [km]</b> 23.5 29.3 97.7 <u>contribution</u> <b>R (km)</b> 23.6	$     \begin{array}{r}         M \\         6.88 \\         7.73 \\         7.07 \\         \hline         \underline{n > 2\%} \\         M \\         7.78 \\         \hline         $	Eps0 0.58	Eps0 [mean values] 1.58 1.53 2.13 Site-to-source azimuth [d] -41.5

Contribution from individual seismic sources to Islamabad (10% PE in 50-years)

## Thank you for your attention

Performance-based Seismic Design of Buildings – Semester: Spring 2020 (Fawad A. Najam)